

1/246

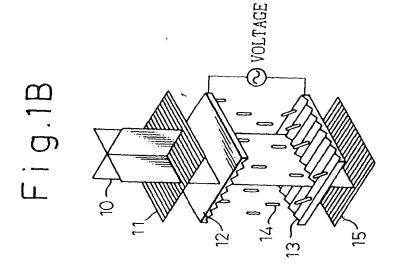
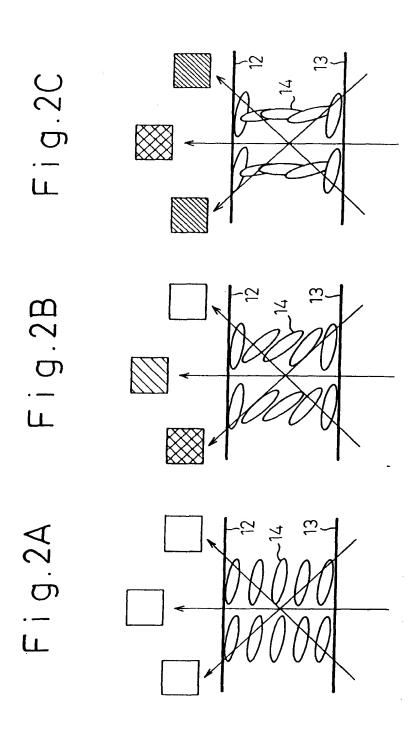


Fig.1A



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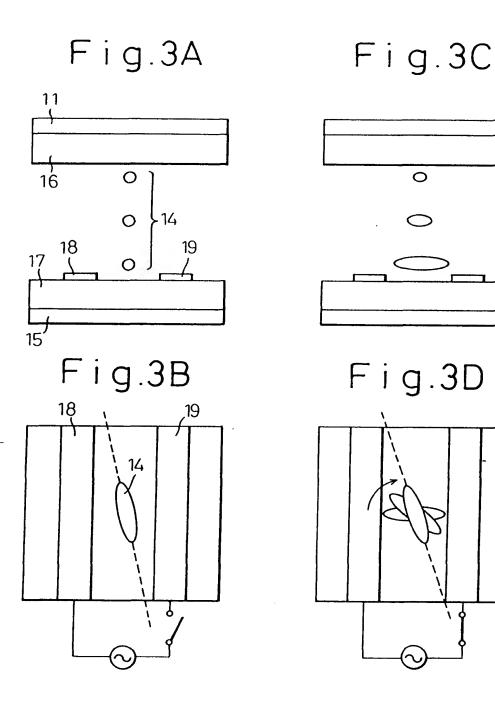
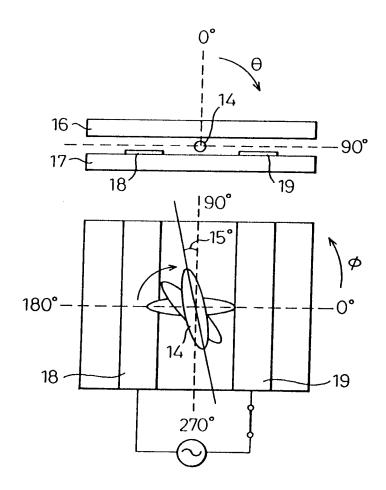


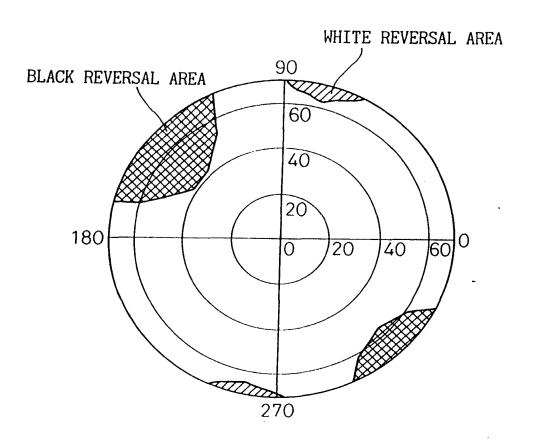


Fig.4

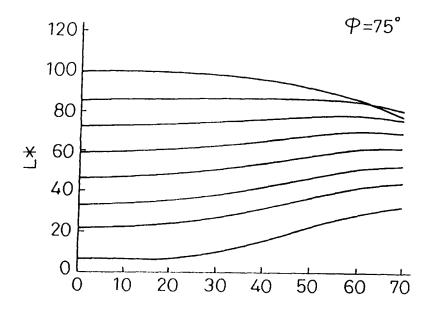


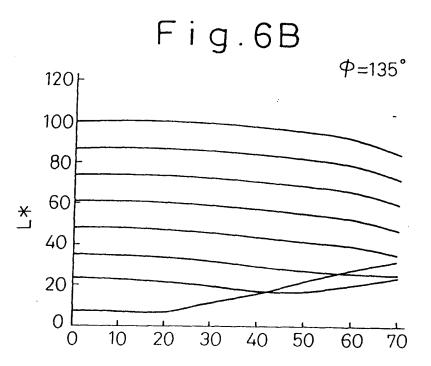
5/246

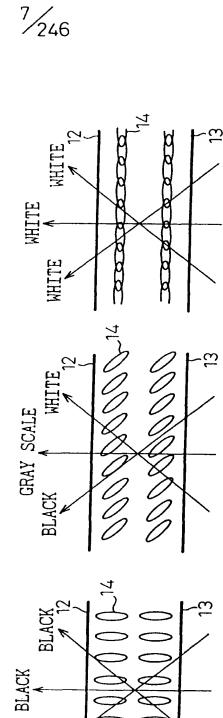
Fig.5



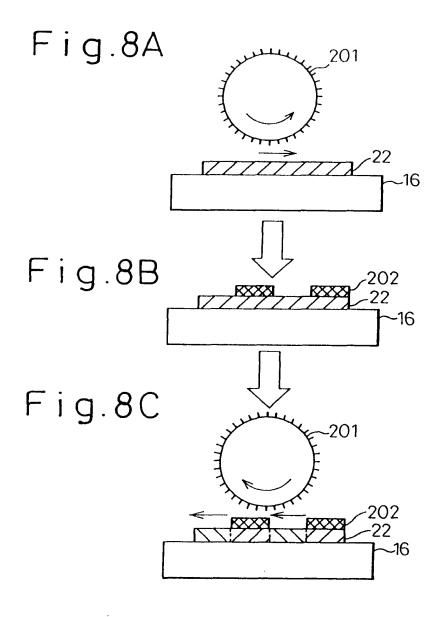
⁶/₂₄₆ Fig.6A

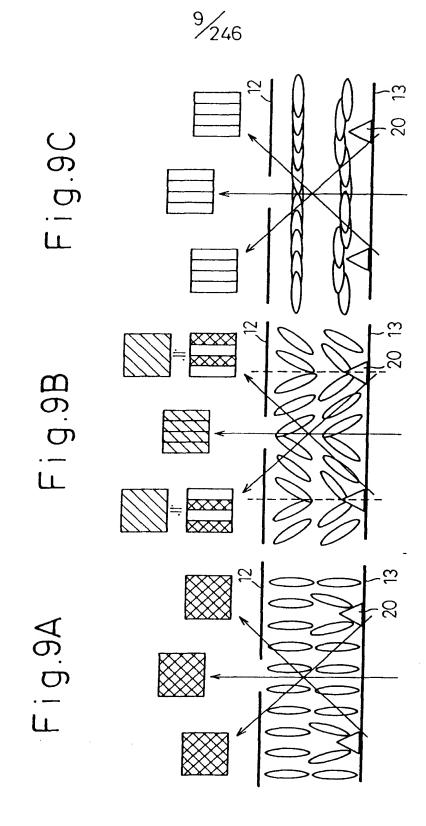




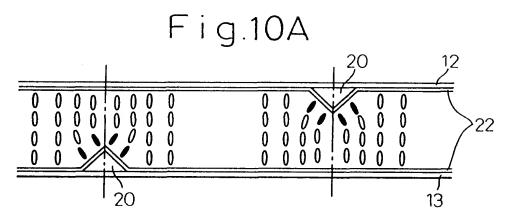












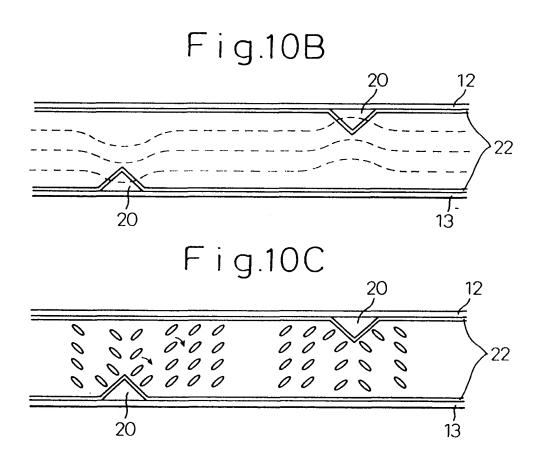


Fig.11A

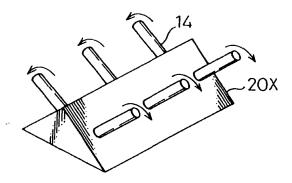


Fig.11B

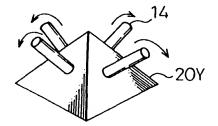
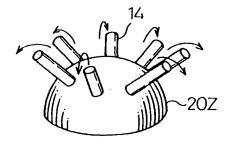


Fig.11C



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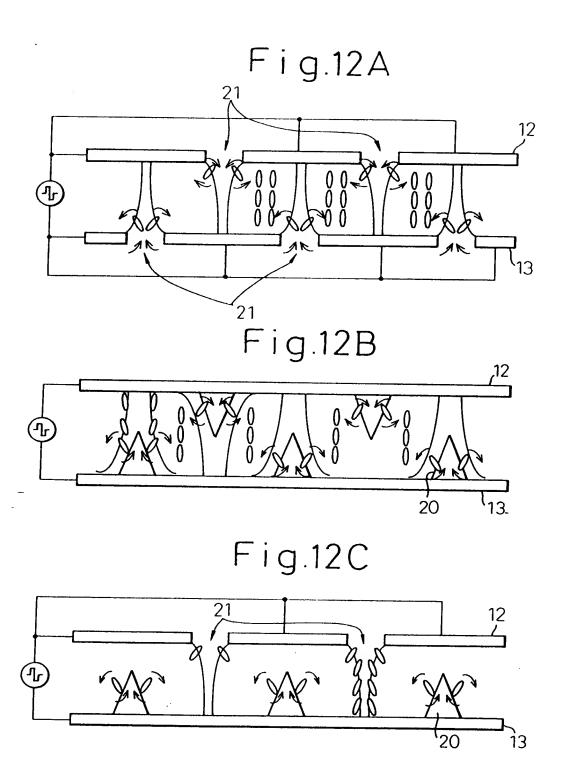




Fig.13

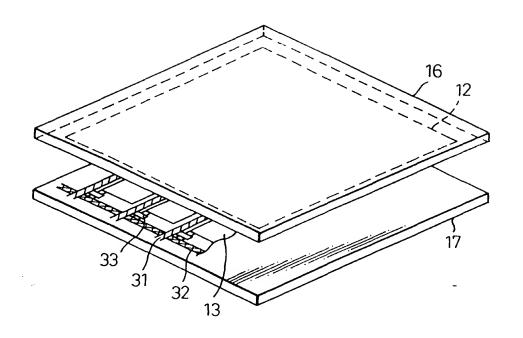


Fig.14A

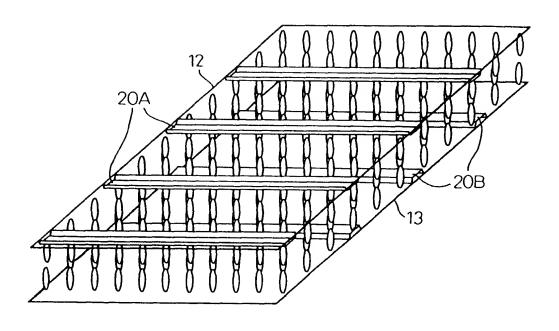


Fig.14B

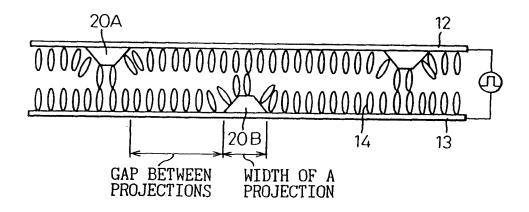


Fig.15

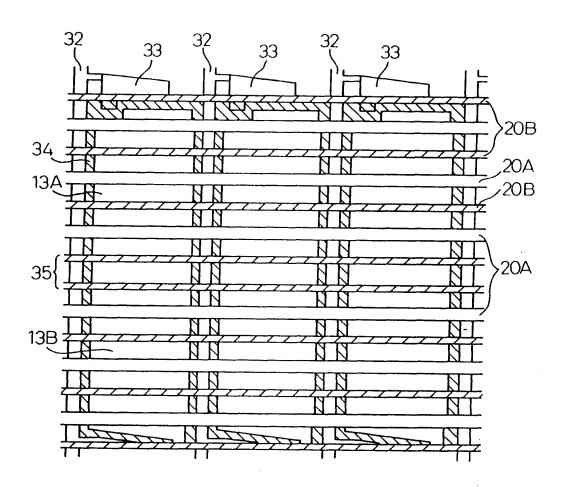
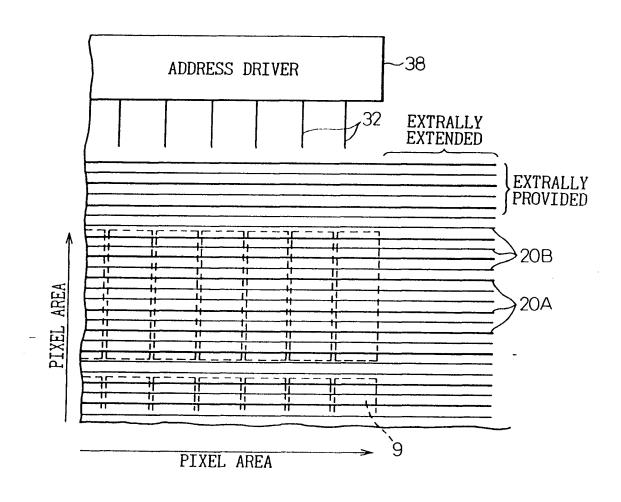
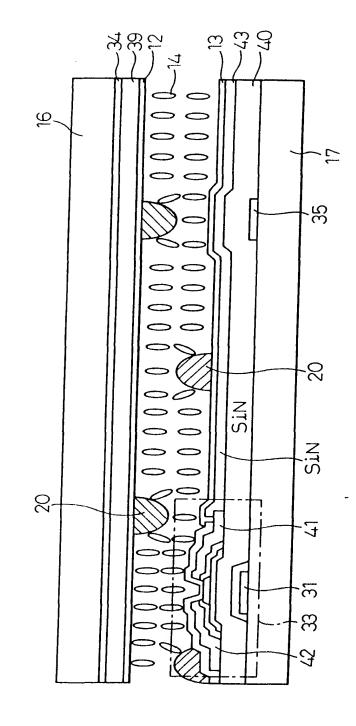




Fig.16



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F i g.17

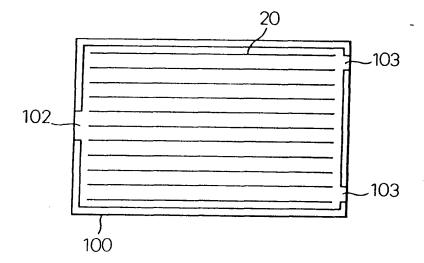
100

Fig.18A

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Fig.18B

101



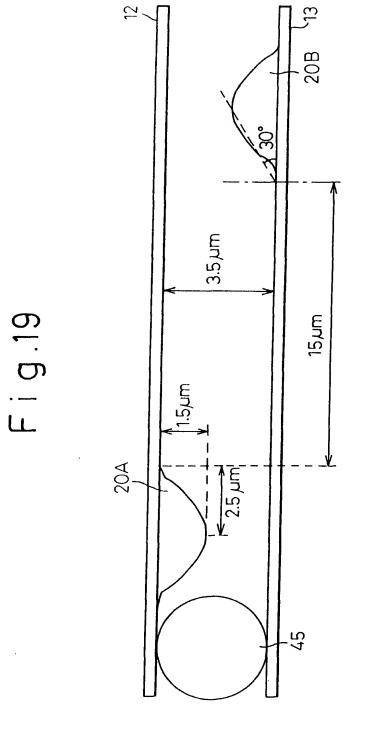
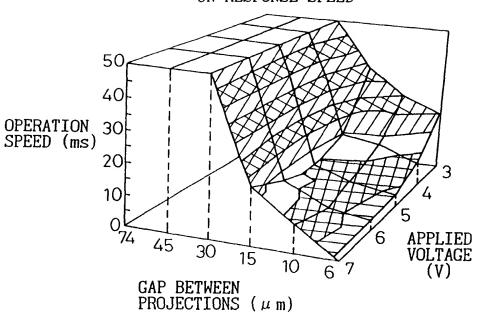


Fig.20A

ON RESPONSE SPEED



OPERATION SPEED (ms) 20

OPERATION SPEED (ms) 20

10

74

45

30

15

10

6

APPLIED VOLTAGE

GAP BETWEEN PROJECTIONS (µm)

Fig.21

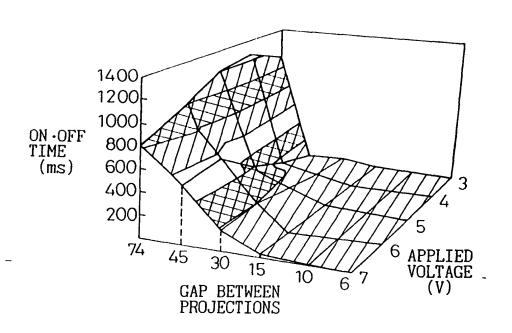
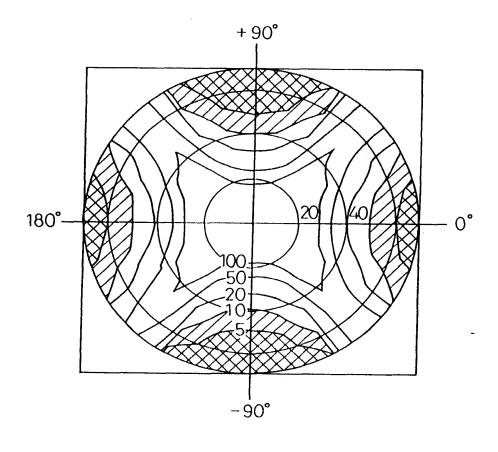
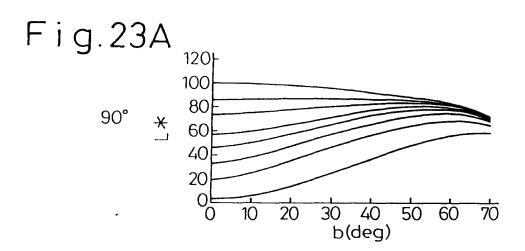
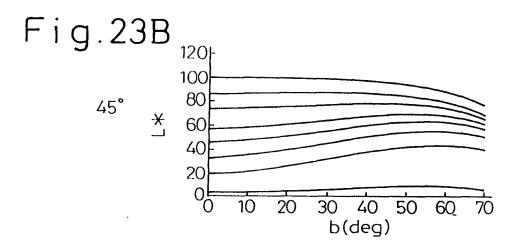


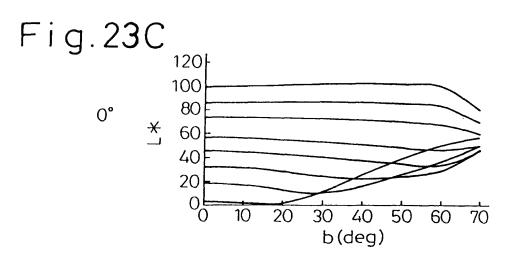


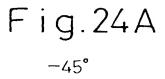
Fig. 22











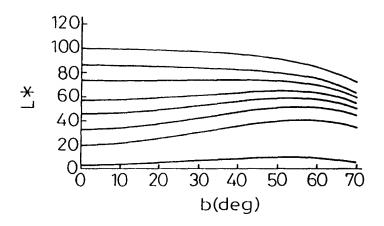


Fig.24B

-90°

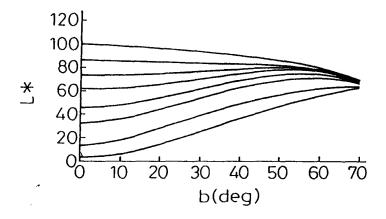
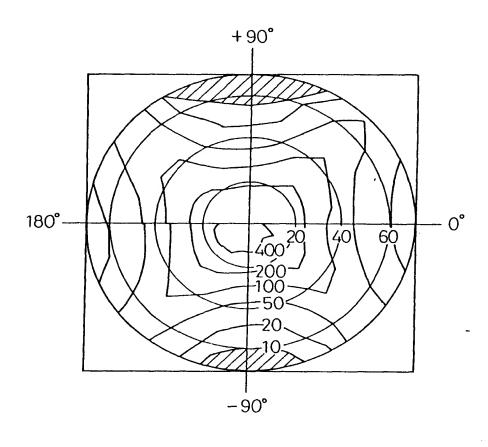


Fig.25



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Fig.26A

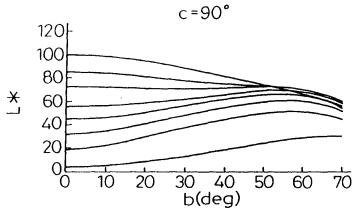


Fig.26B

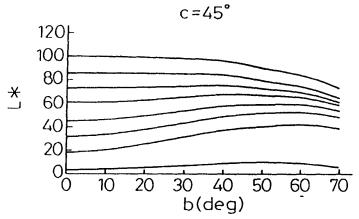


Fig.26C

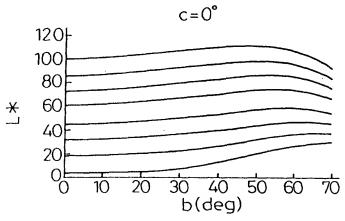
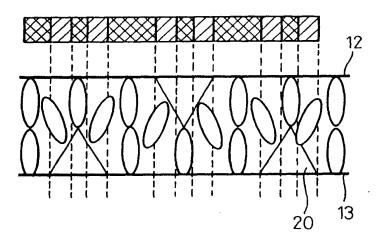
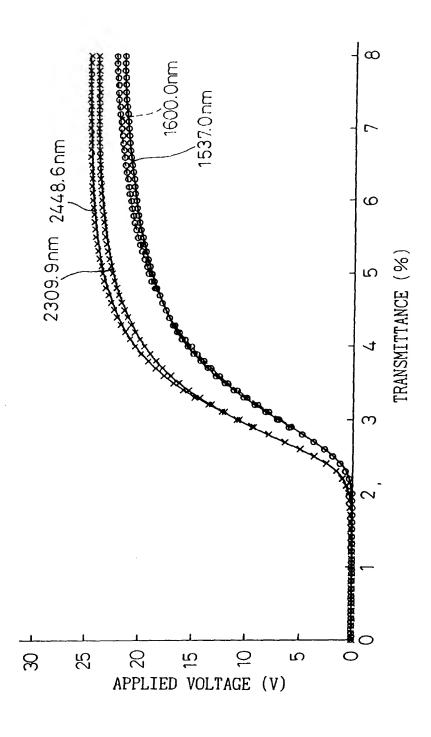


Fig.27

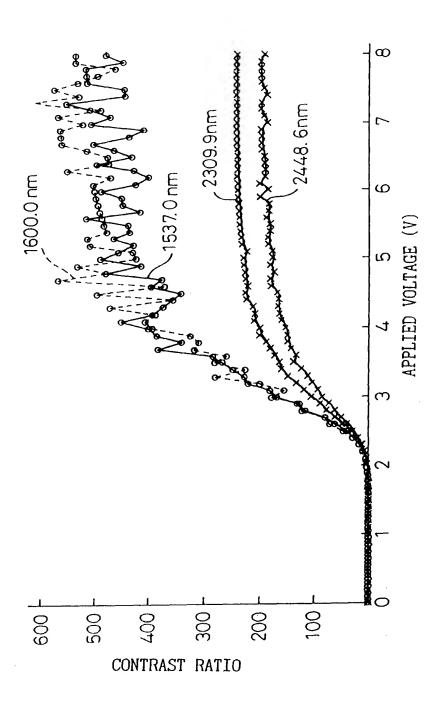


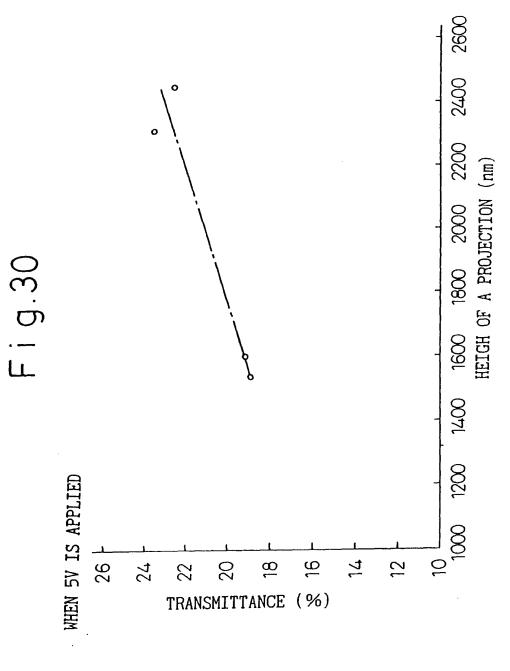
1.01 Cart 1 18 Safe Ball for and mile 1 1 10 Cart 1 10 The Cart 1 10 The



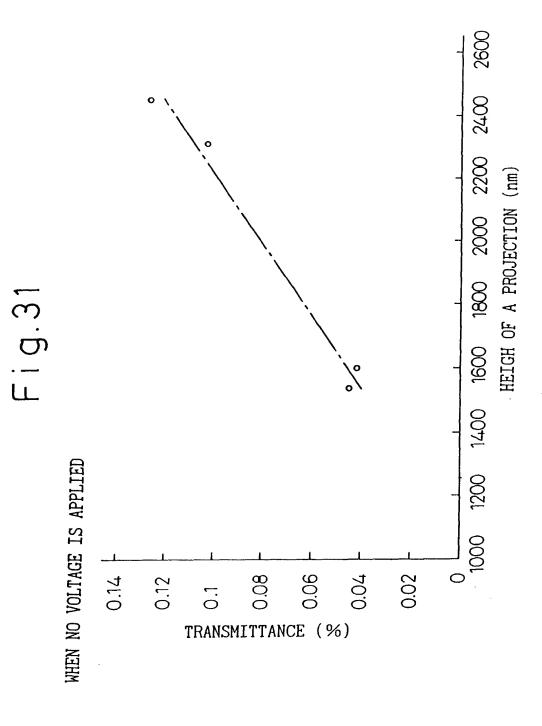












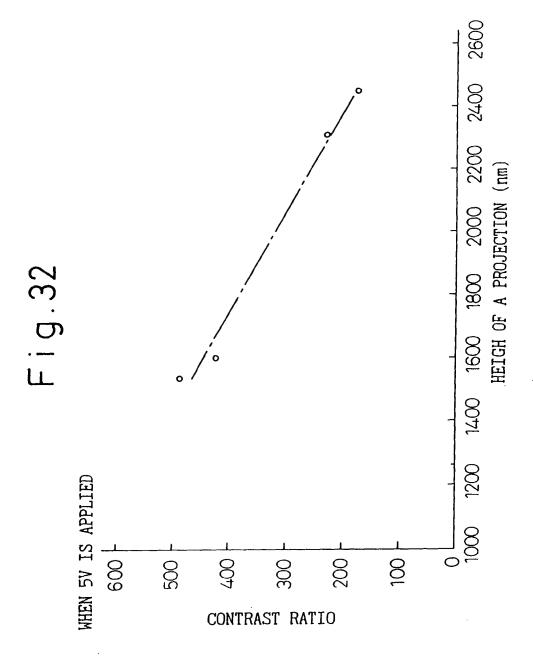




Fig.33

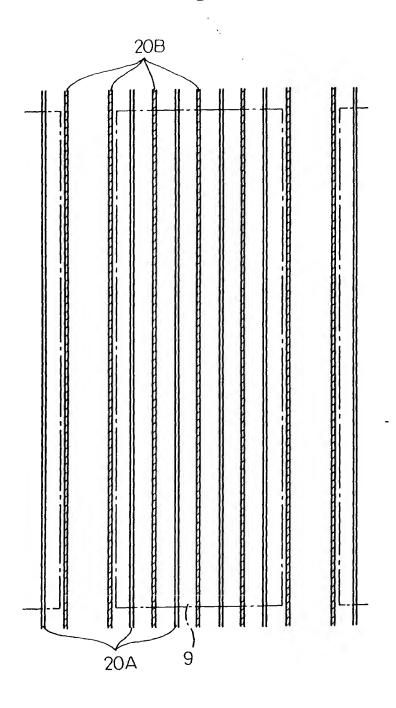




Fig.34

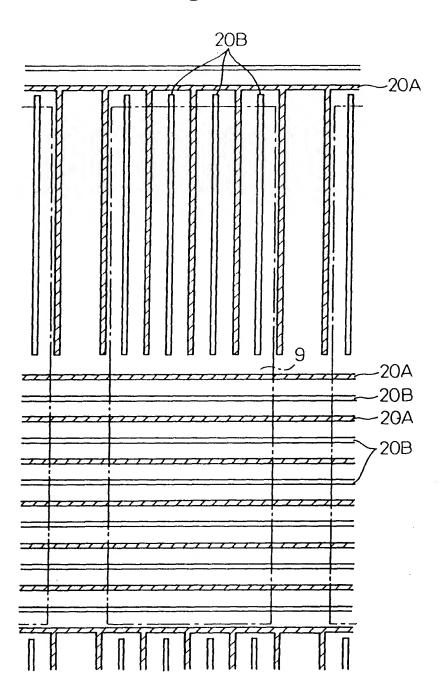




Fig.35

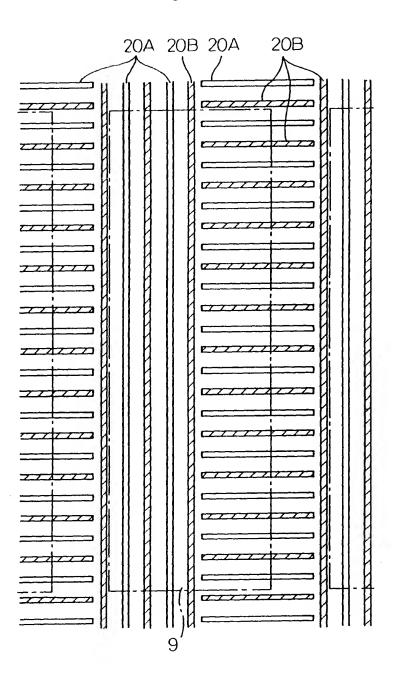




Fig.36

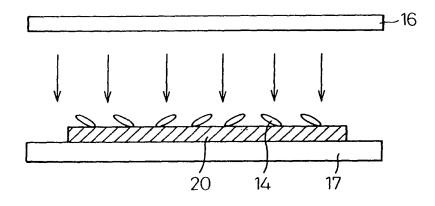


Fig.37A

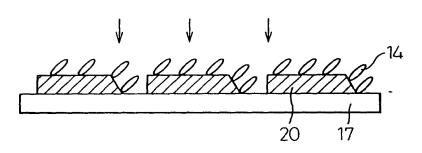


Fig.37B

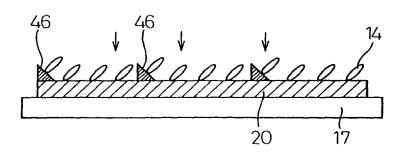


Fig.38A

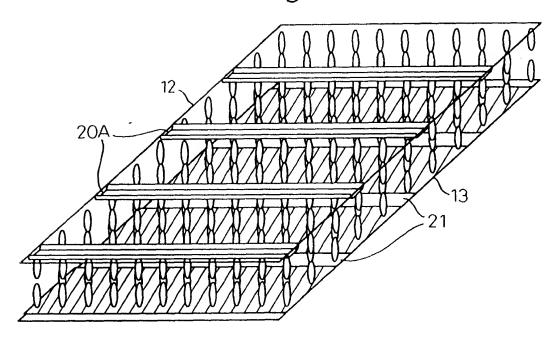


Fig.38B

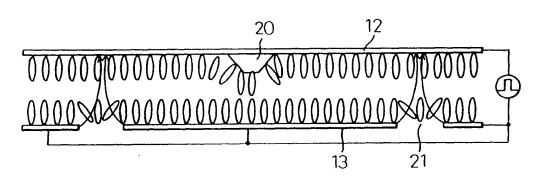
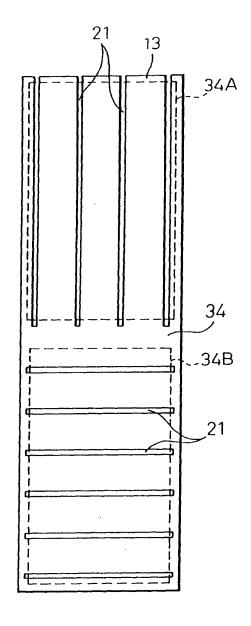


Fig.39



³⁹/₂₄₆

Fig.40

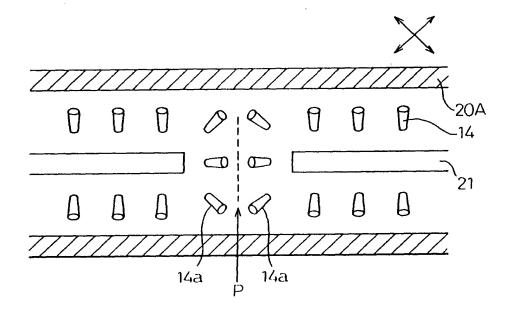


Fig.41

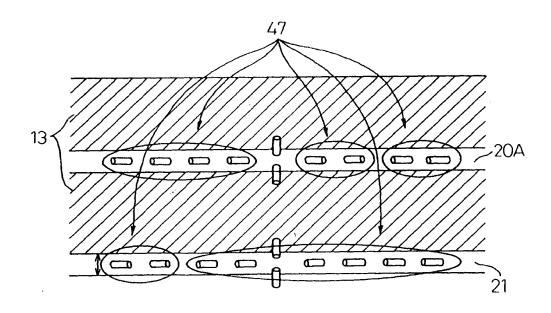


Fig. 42

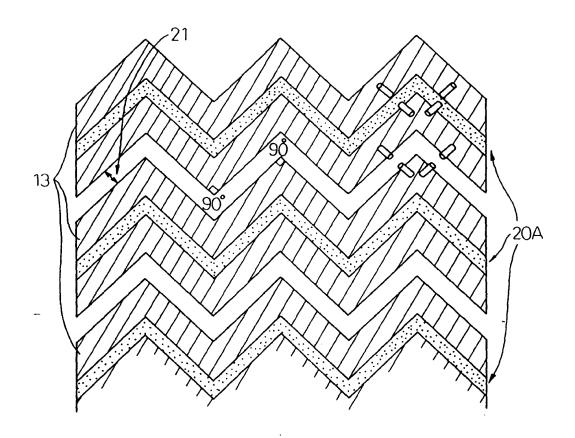
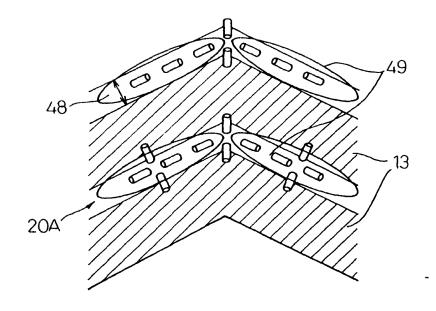




Fig.43



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⁴²/₂₄₆ Fig.44

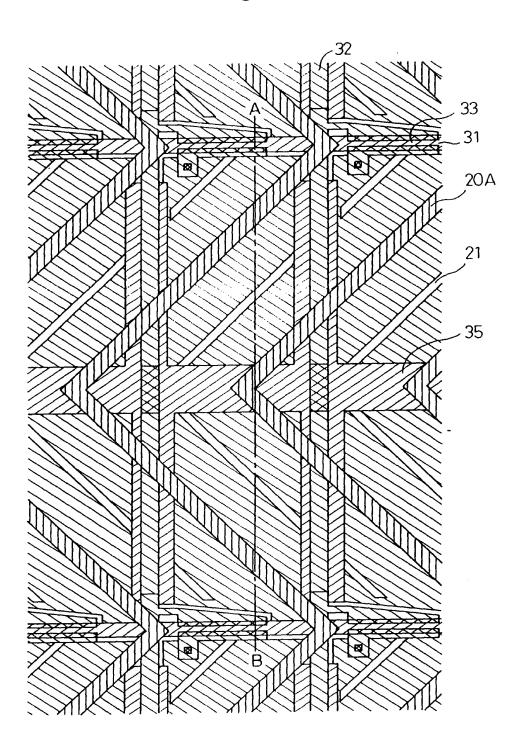
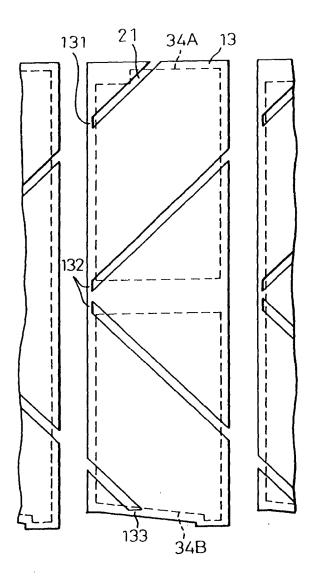
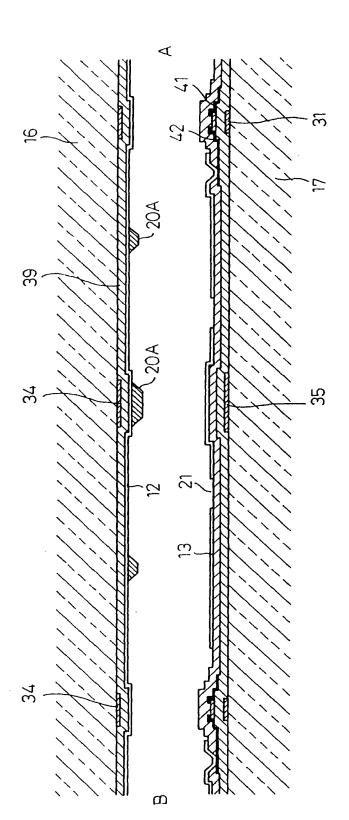




Fig.45



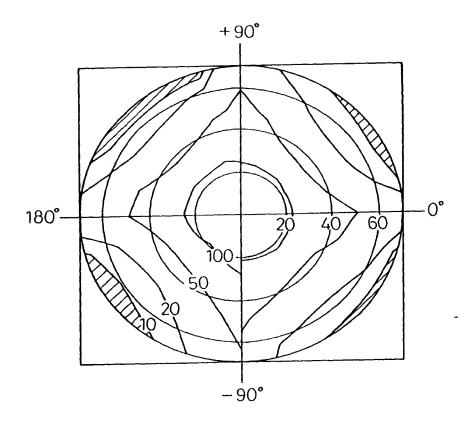
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F i g.46



Fig.47



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Fig.48A

-90°

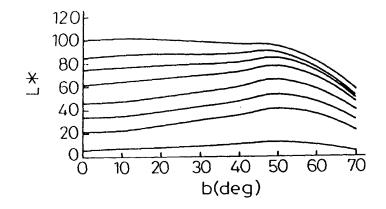


Fig.48B

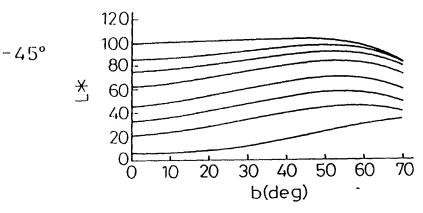


Fig.48C

O°

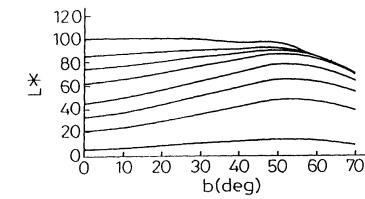


Fig.49A

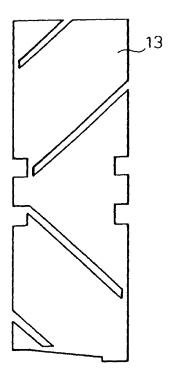
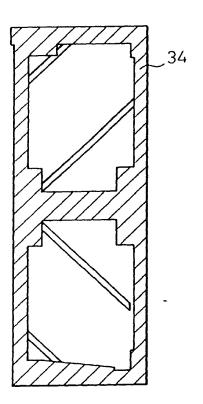
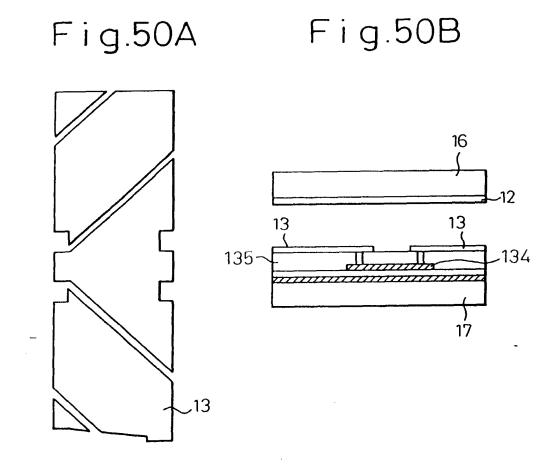


Fig.49B

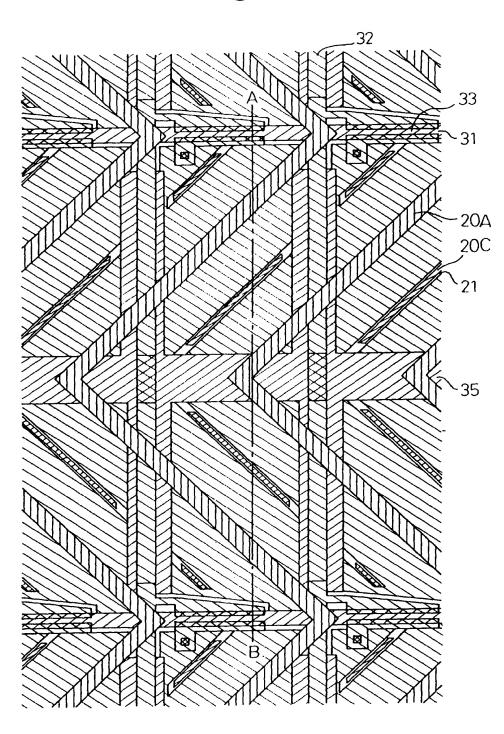


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Fig.51



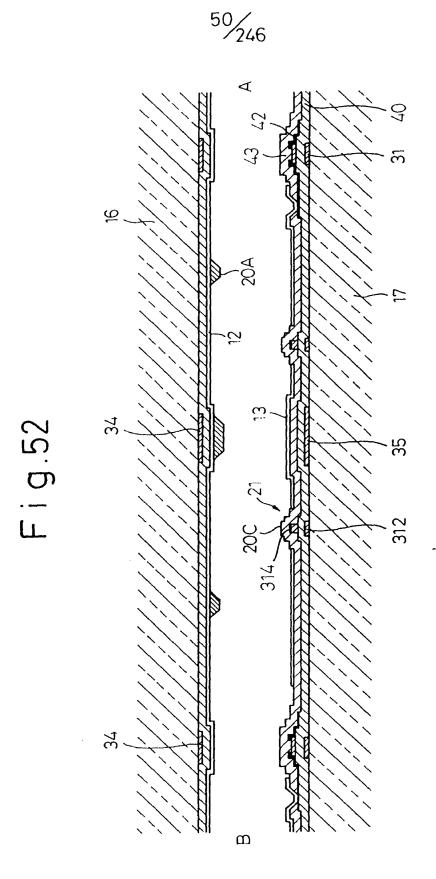




Fig.53A

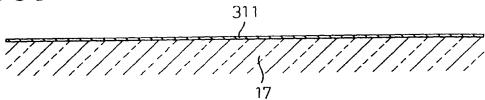


Fig. 53B

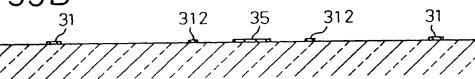


Fig.53C

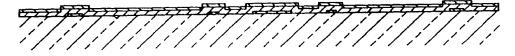
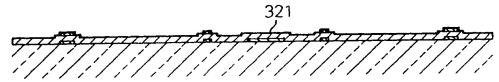


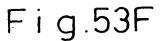
Fig.53D



Fig.53E







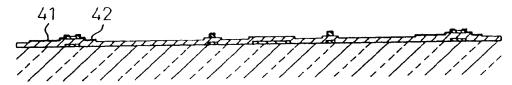


Fig.53G

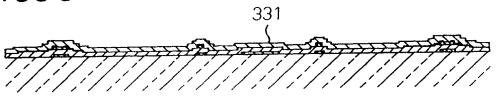


Fig.53H

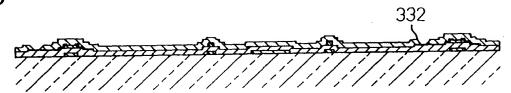


Fig.53I

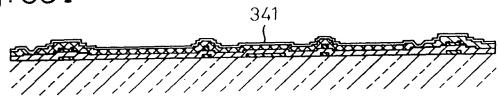


Fig. 53,J

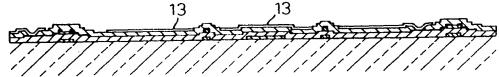
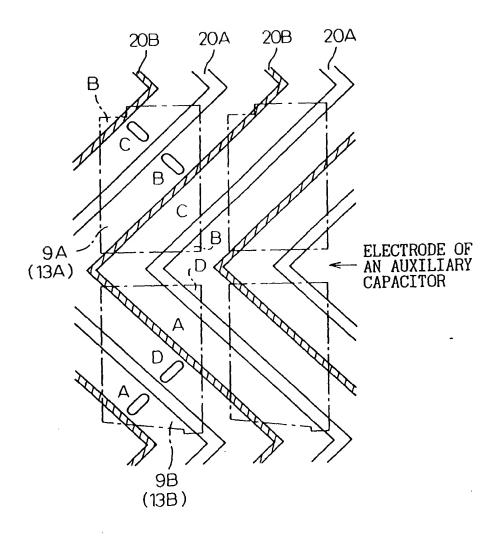




Fig.54



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Fig.55

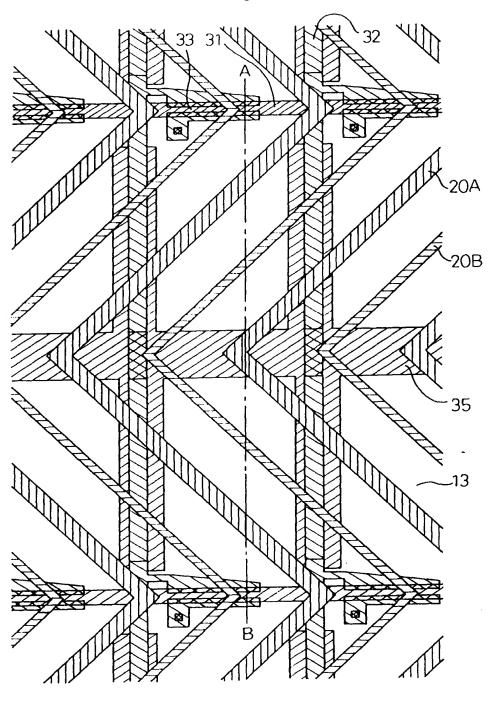




Fig.56

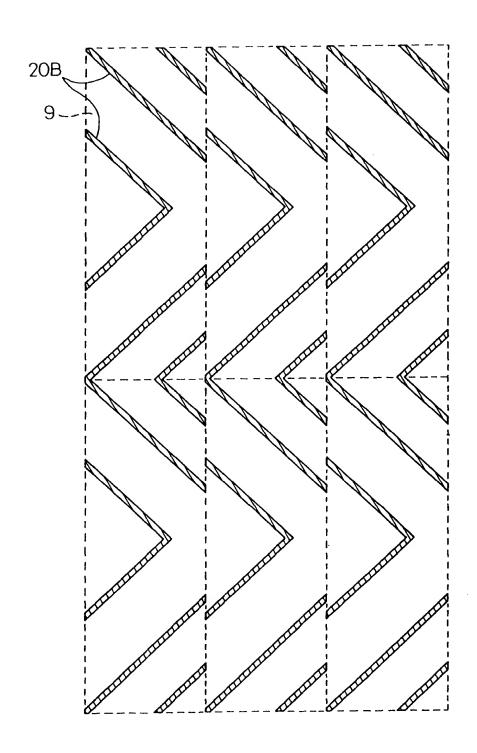




Fig.57A

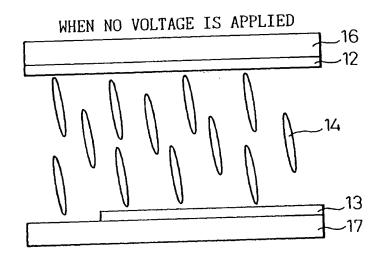


Fig.57B

WHEN A VOLTAGE IS APPLIED

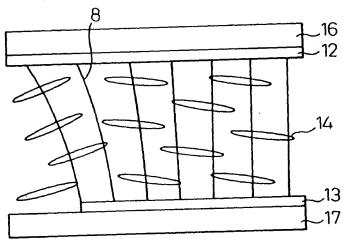
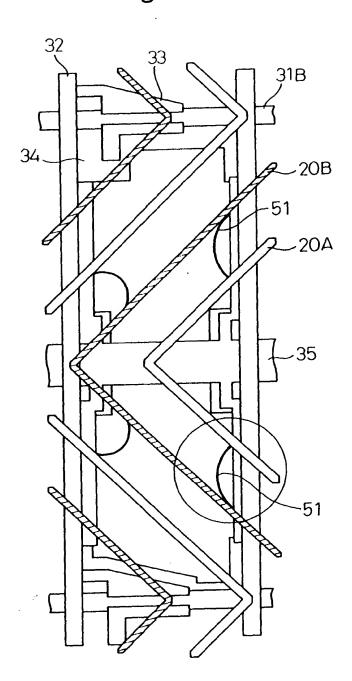




Fig.58



58/₂₄₆

Fig.59

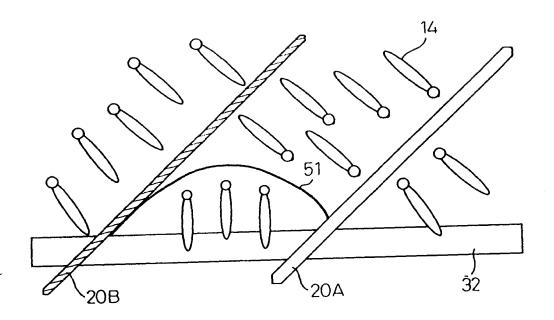




Fig. 60

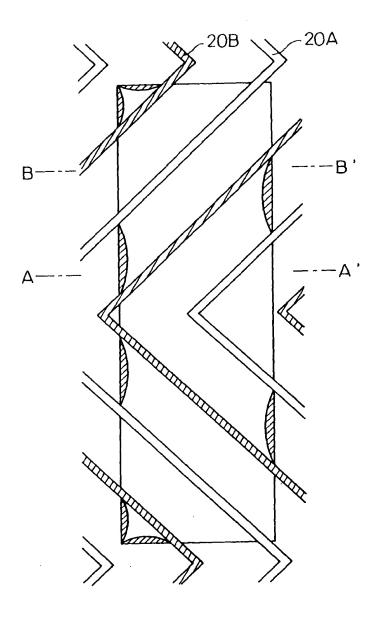


Fig.61A

A - A,

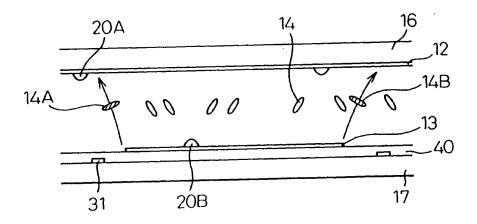


Fig.61B

B-B'

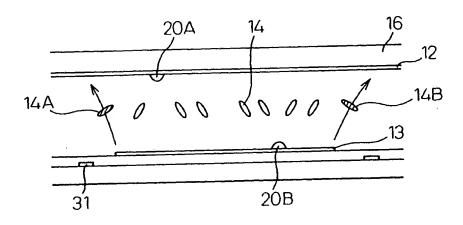




Fig.62A

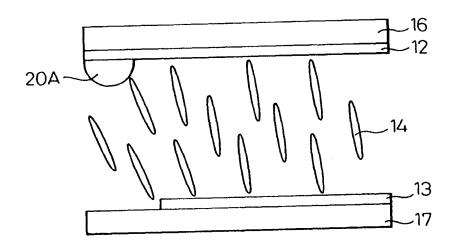


Fig.62B

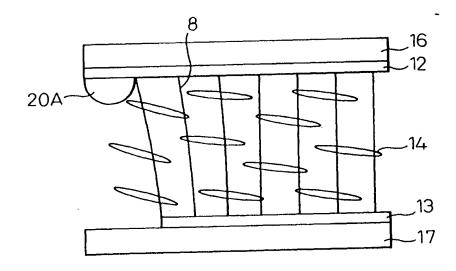




Fig. 63

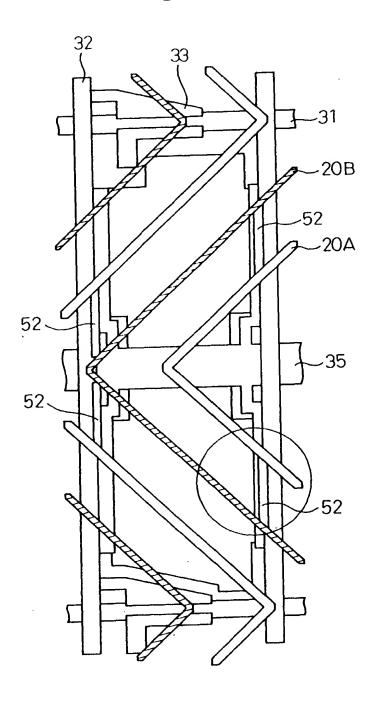




Fig.64

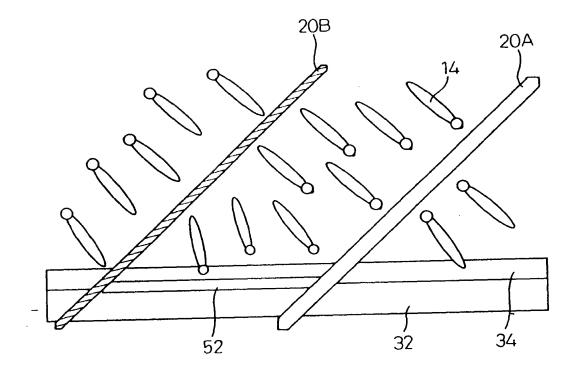




Fig.65A

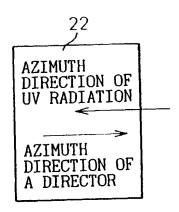
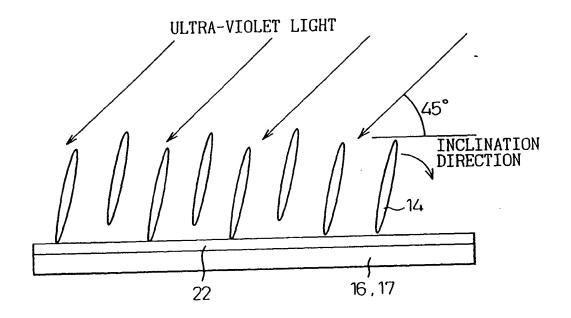


Fig.65B



65/₂₄₆

Fig.66

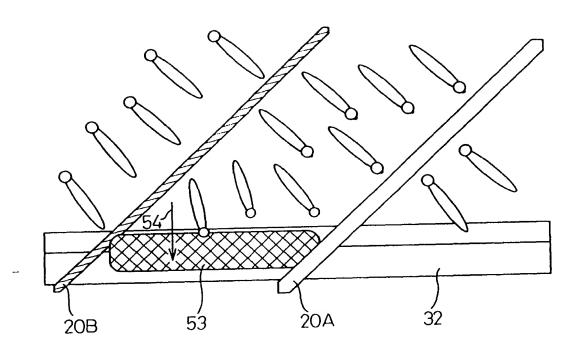




Fig.67A

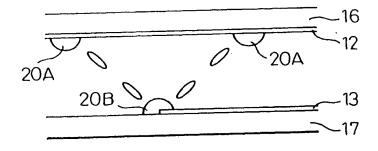


Fig.67B

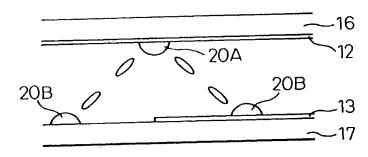


Fig.67C

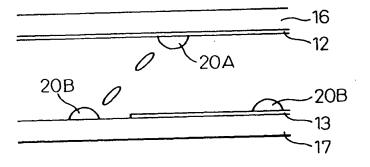




Fig.68

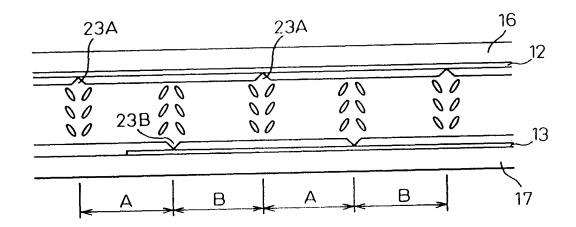




Fig.69A

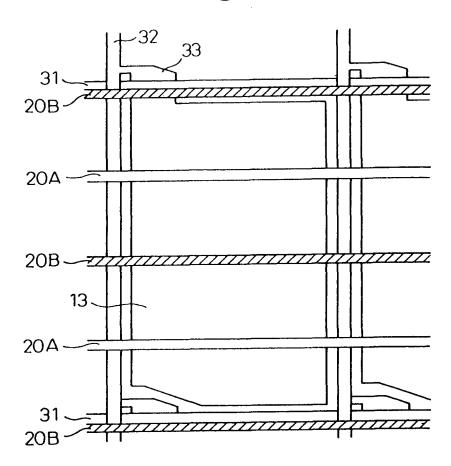


Fig.69B

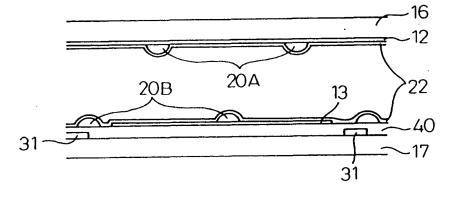




Fig.70A

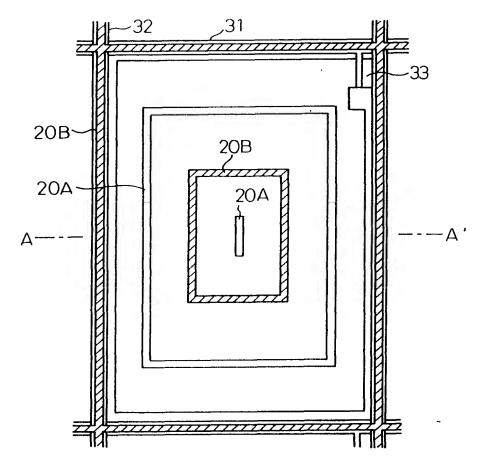


Fig.70B

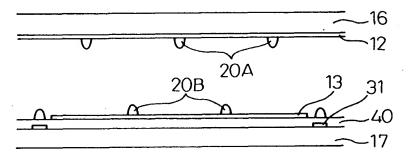




Fig.71

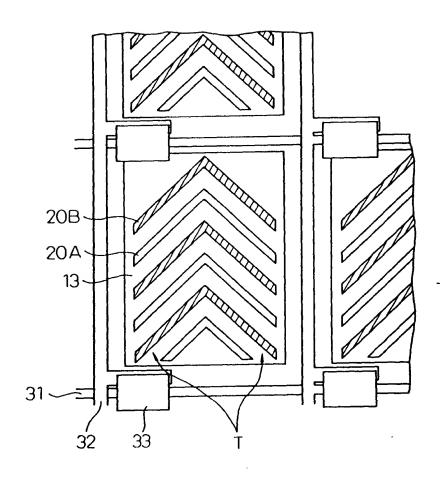




Fig.72

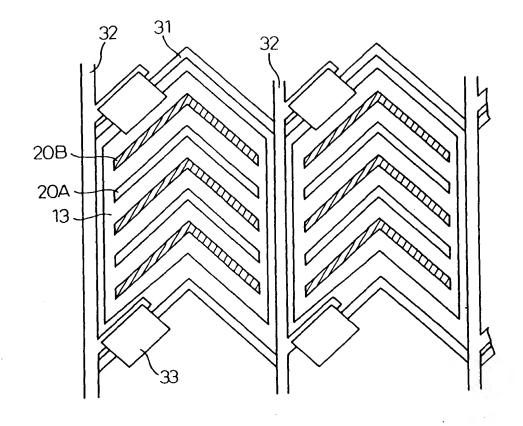




Fig.73

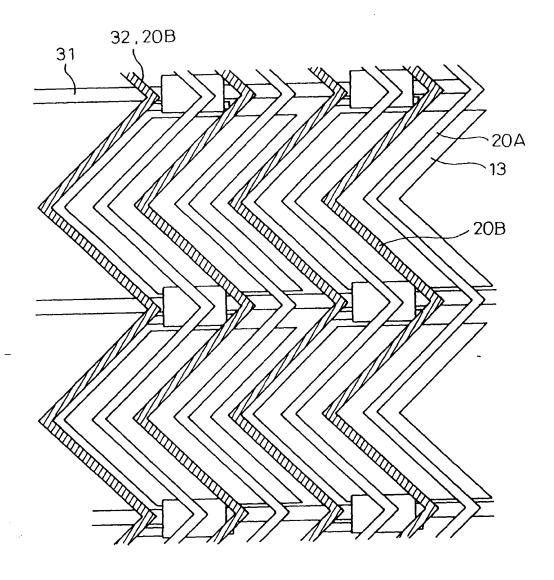






Fig.74

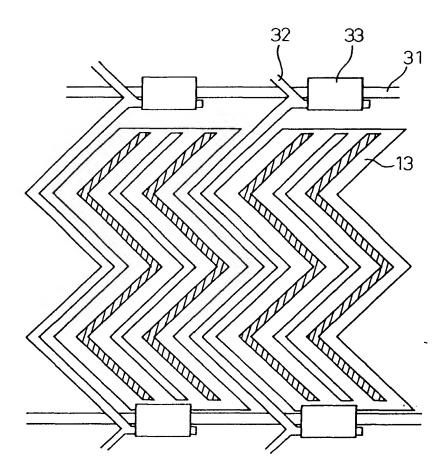
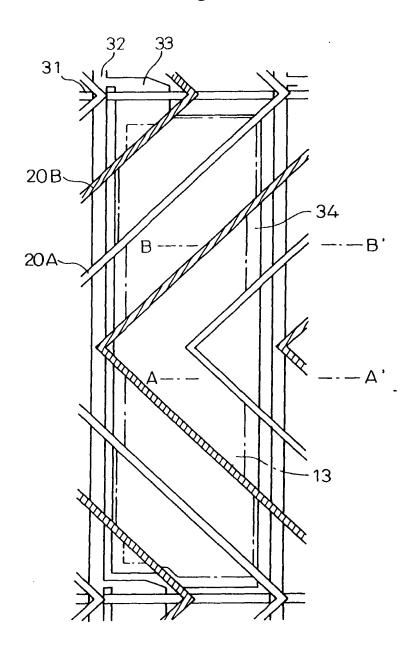
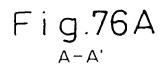




Fig.75







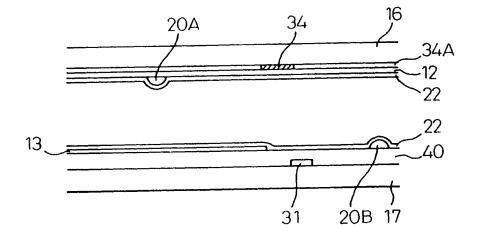


Fig.76B

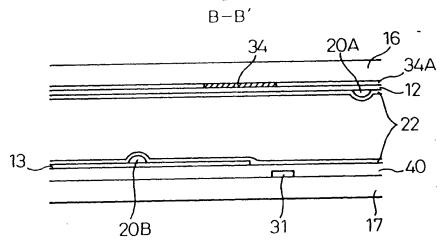




Fig.77A

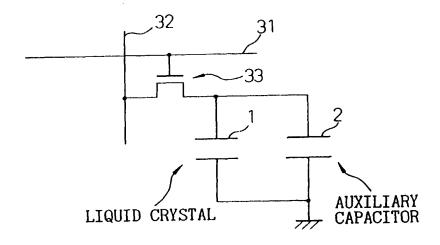


Fig.77B

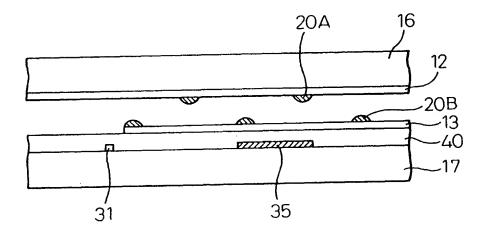




Fig.78A

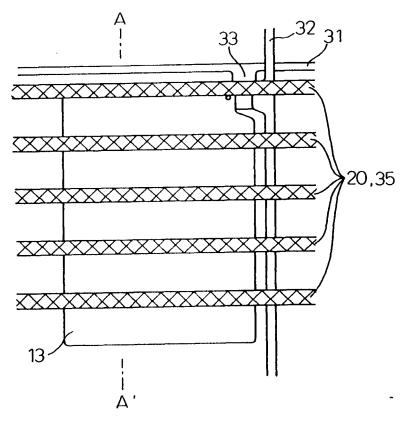




Fig.79A

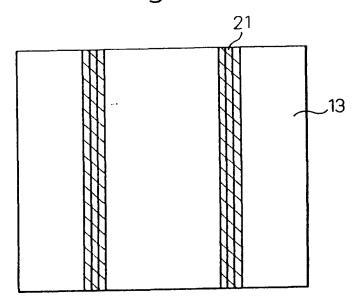


Fig.79B

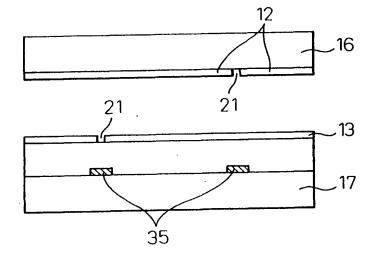




Fig.80A

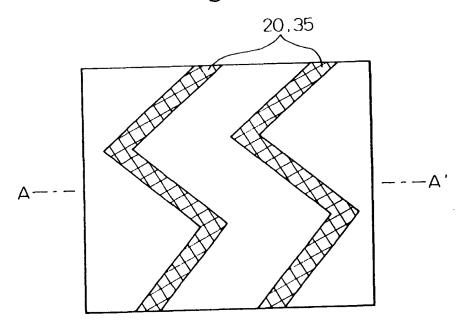


Fig.80B

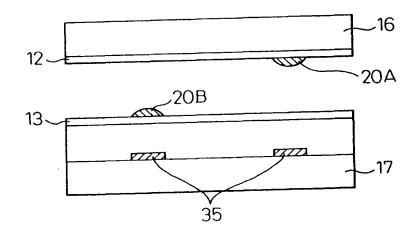




Fig.81A

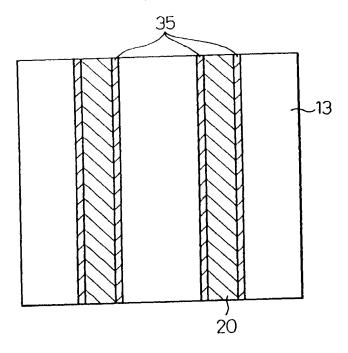


Fig.81B

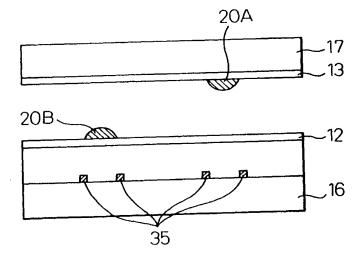
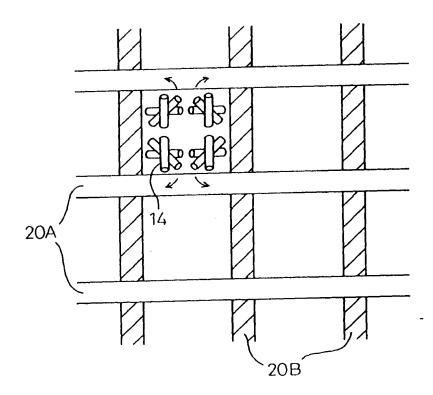




Fig.82





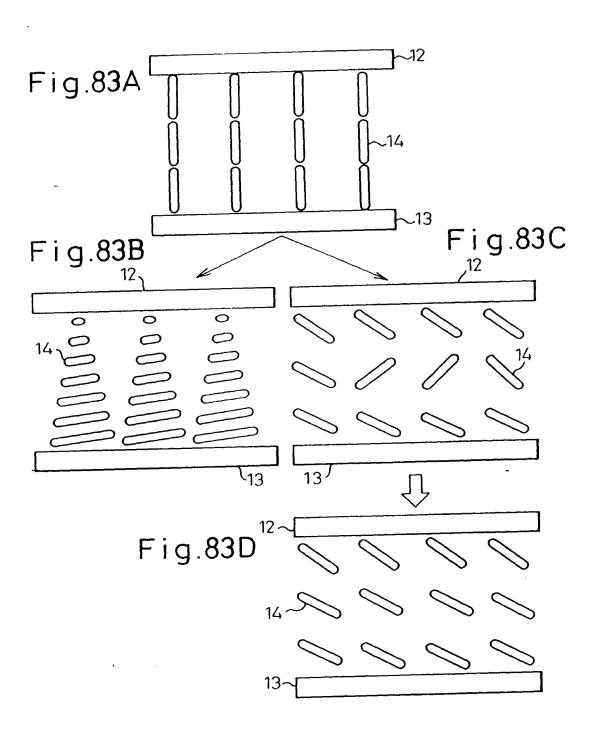
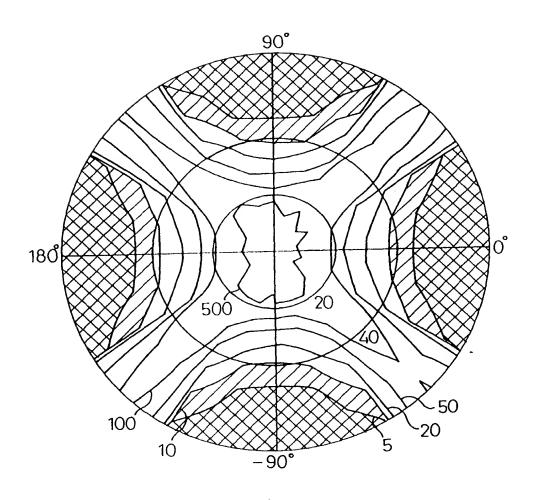
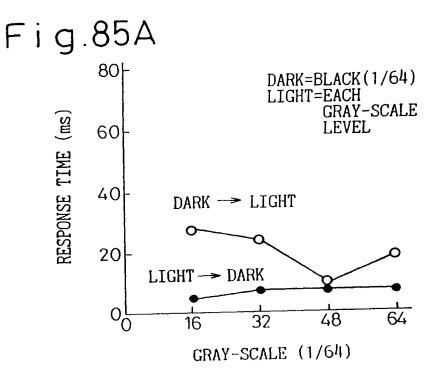




Fig.84







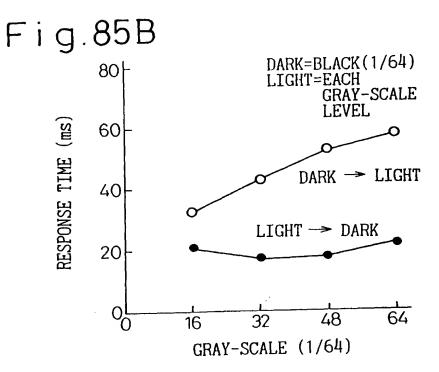




Fig.85C

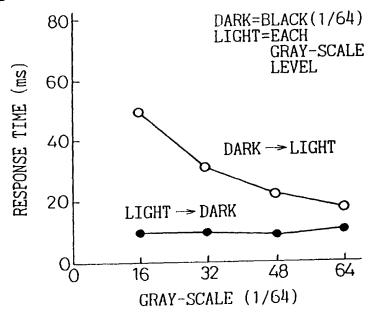
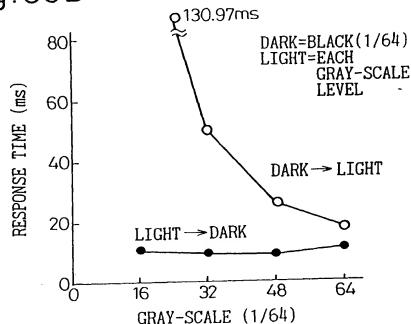
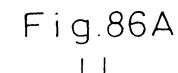


Fig.85D







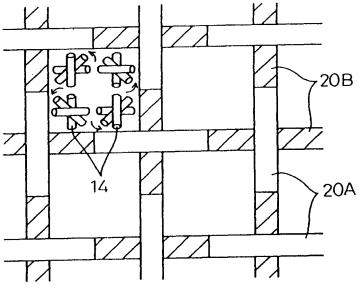


Fig.86B

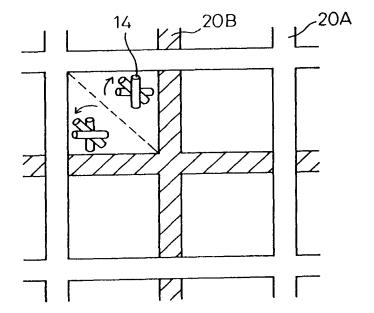




Fig.87

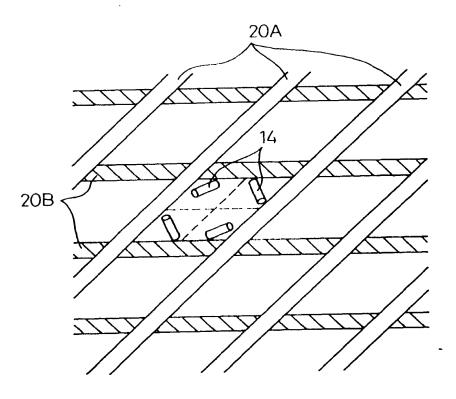




Fig.88

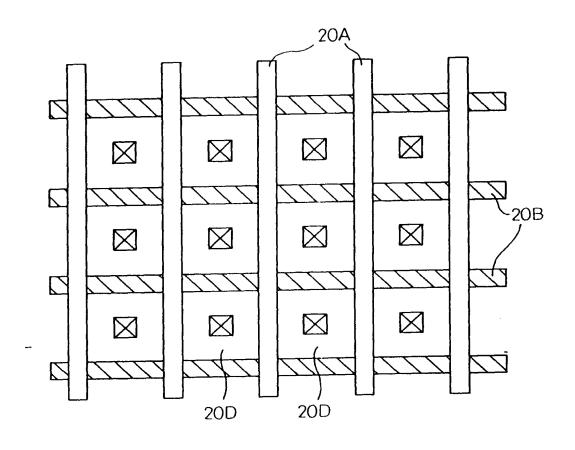




Fig.89

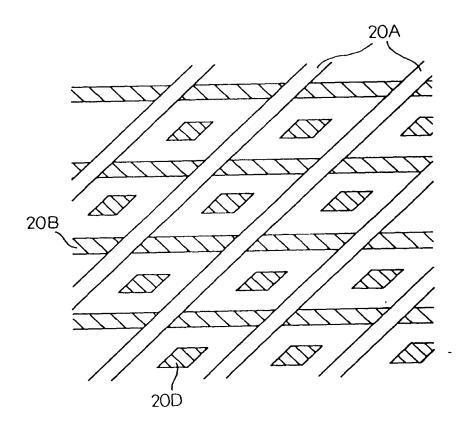




Fig.90A

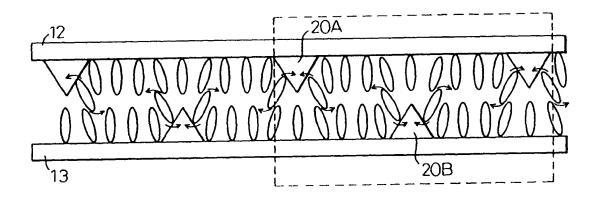


Fig.90B

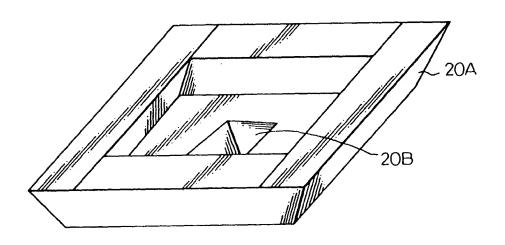




Fig.91

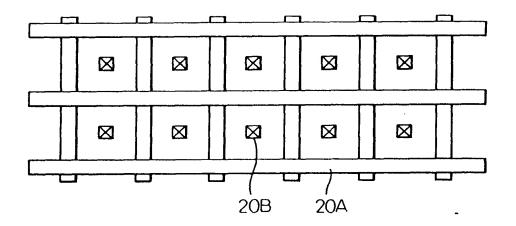




Fig.92A

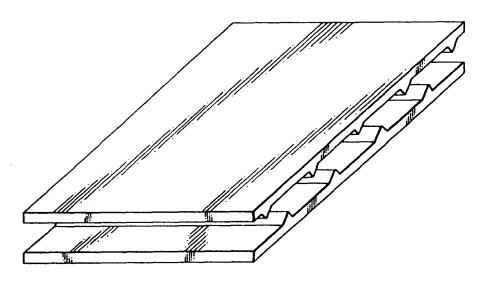


Fig.92B

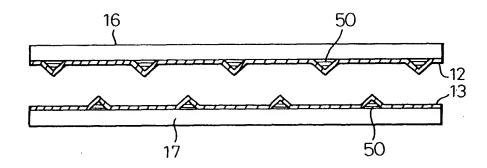




Fig.93

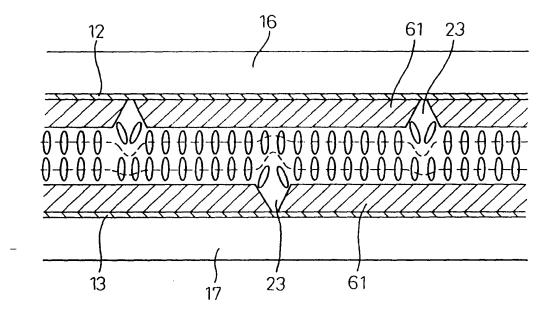




Fig.94

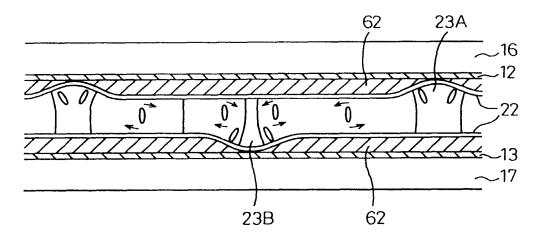


Fig.95

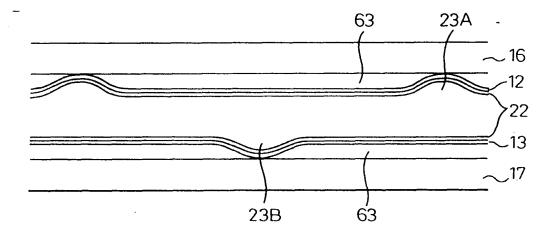




Fig.96

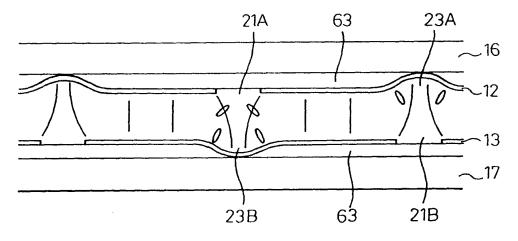


Fig.97

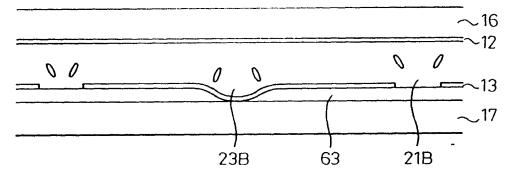


Fig.98

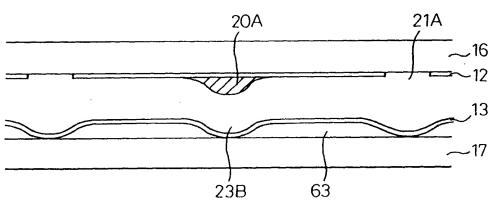




Fig.99A

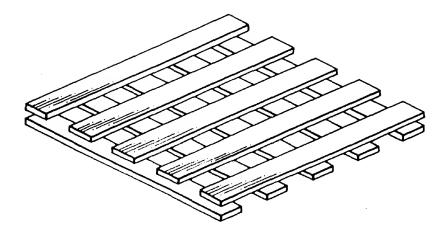
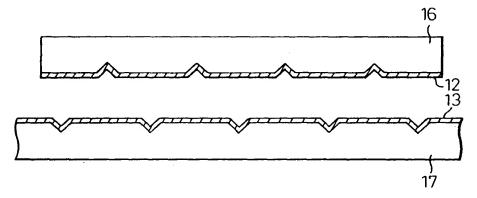


Fig.99B





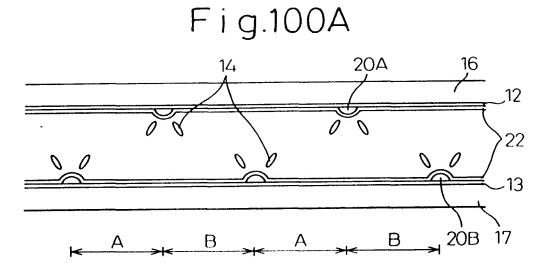


Fig.100B

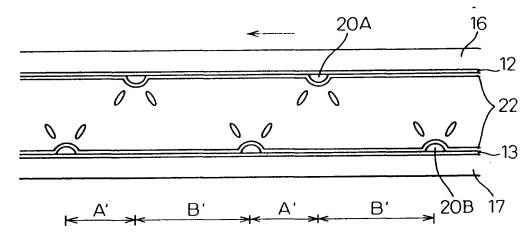




Fig.101A

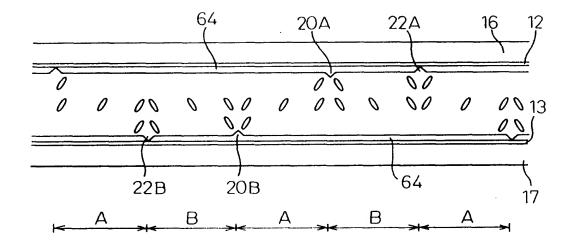


Fig.101B

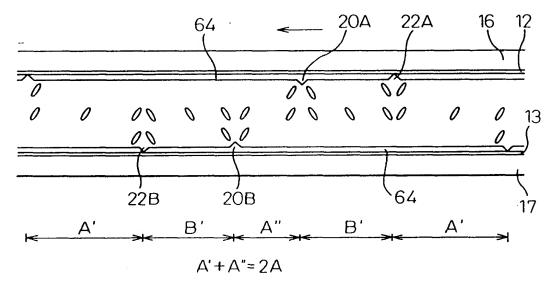




Fig.102

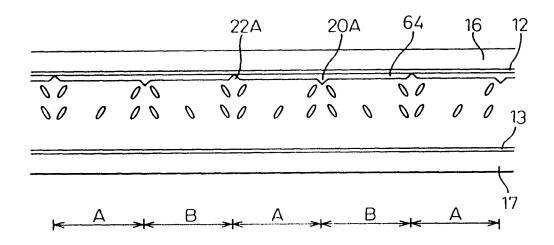




Fig.103A

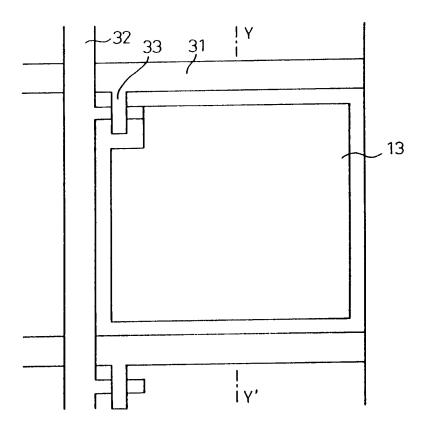


Fig. 103B

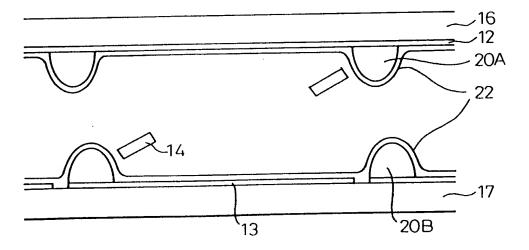
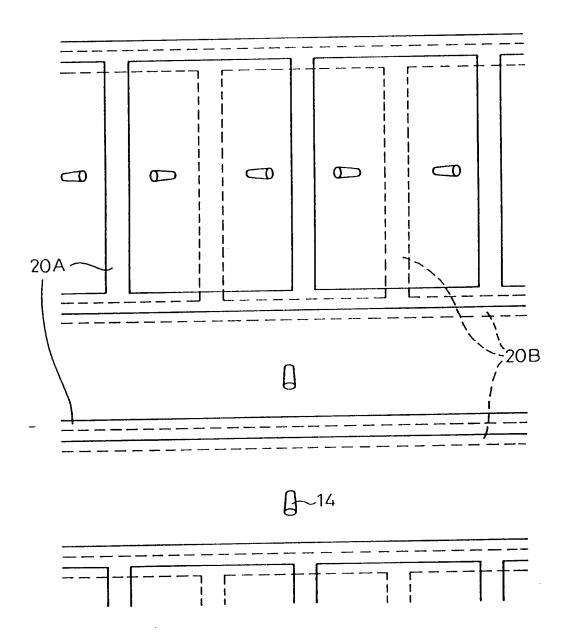




Fig.104





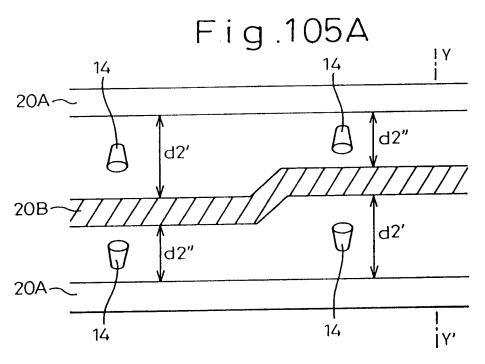


Fig.105B

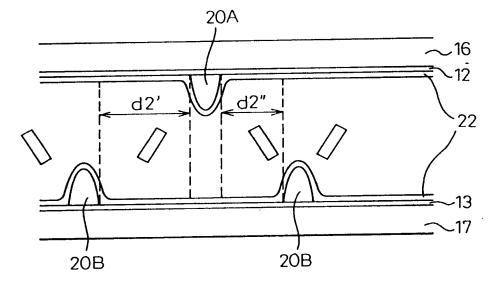




Fig.106

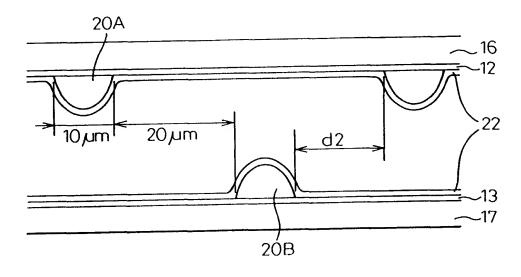


Fig.107

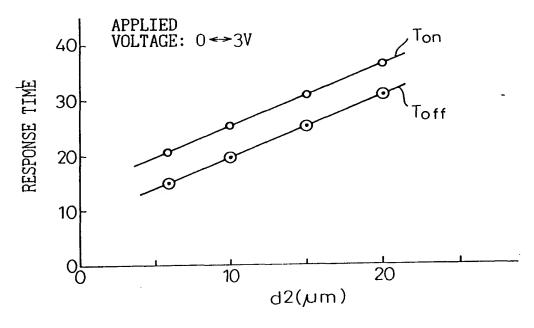




Fig.108A

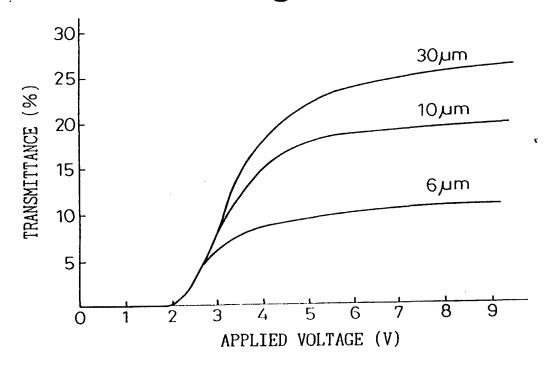


Fig.108B

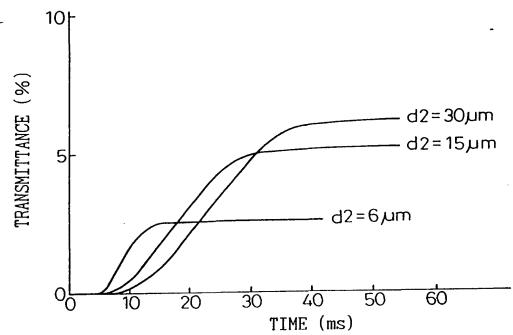




Fig.109A

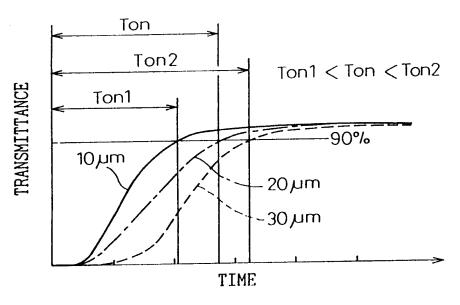


Fig.109B

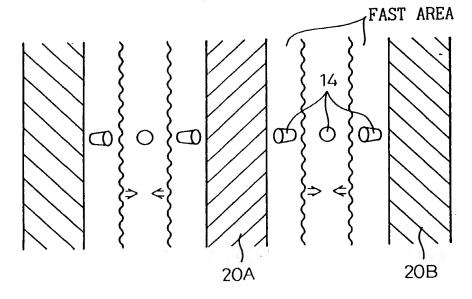




Fig.110

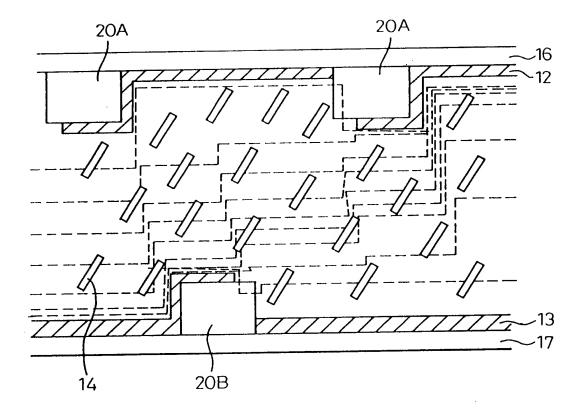




Fig.111

CONTRAST	RATIO
	100.000 50.000 20.000 10.000 5.000

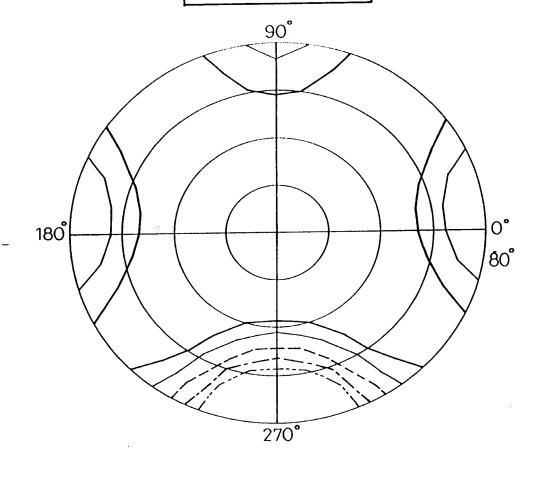




Fig.112

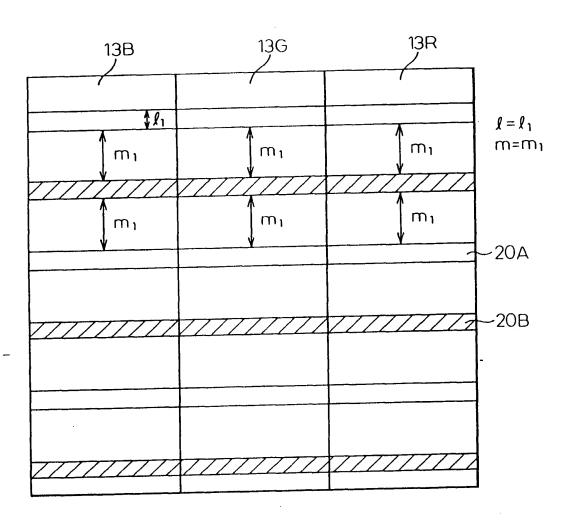
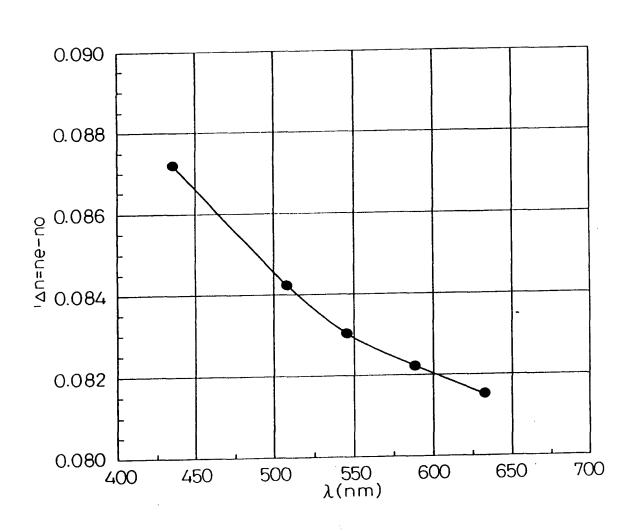


Fig.113



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Fig.114

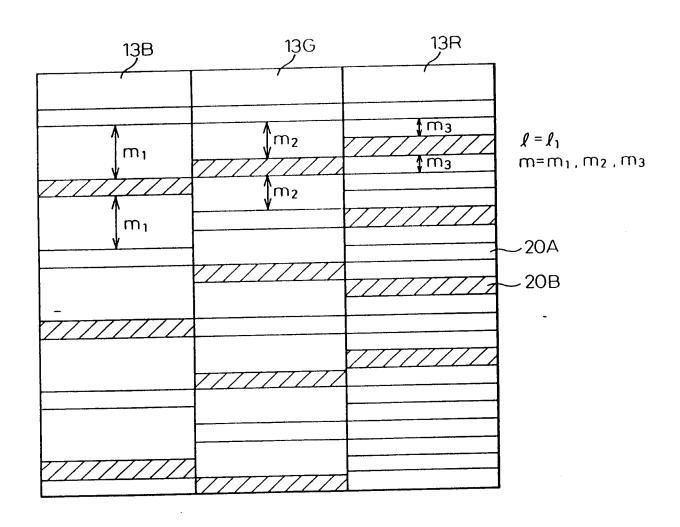




Fig.115

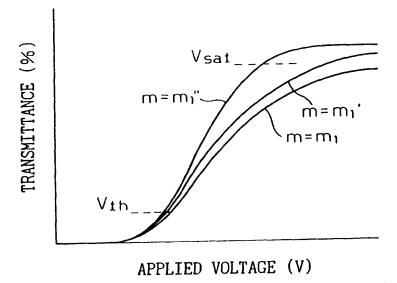


Fig.116

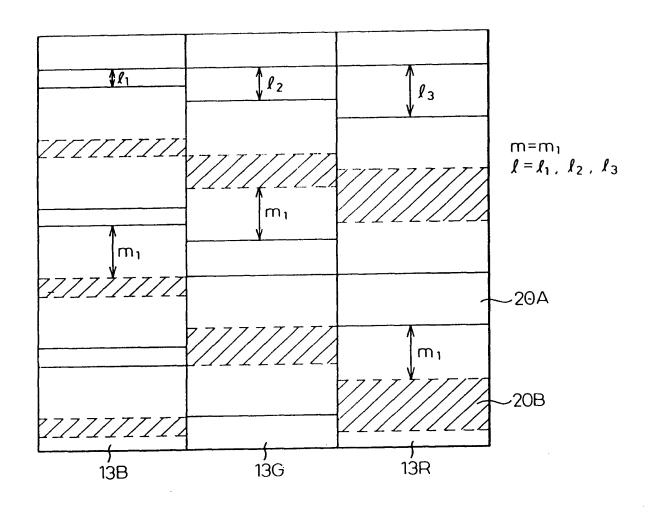




Fig.117

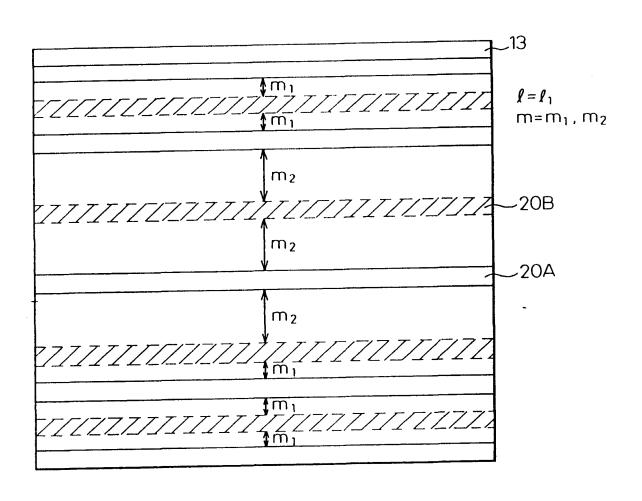
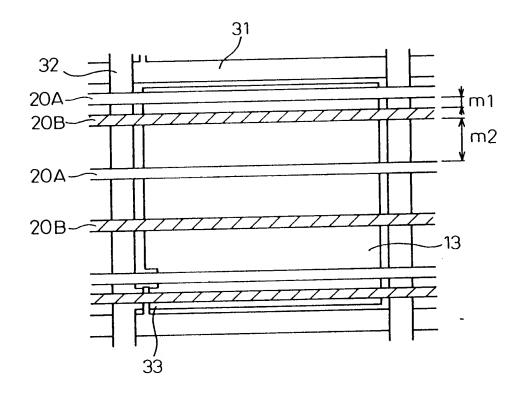




Fig.118



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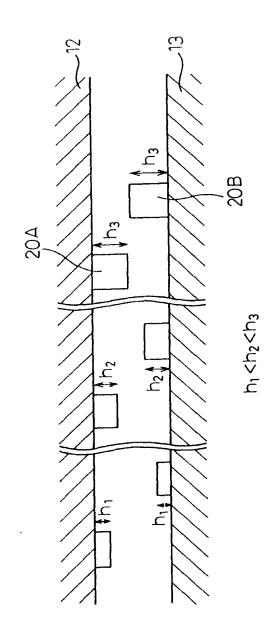


Fig.119



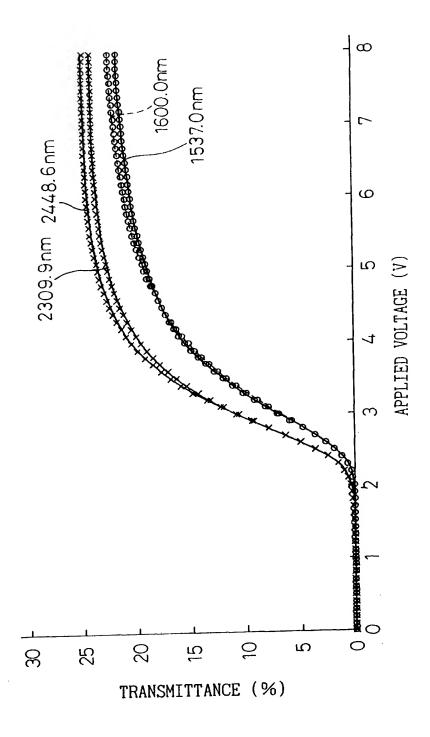


Fig.120

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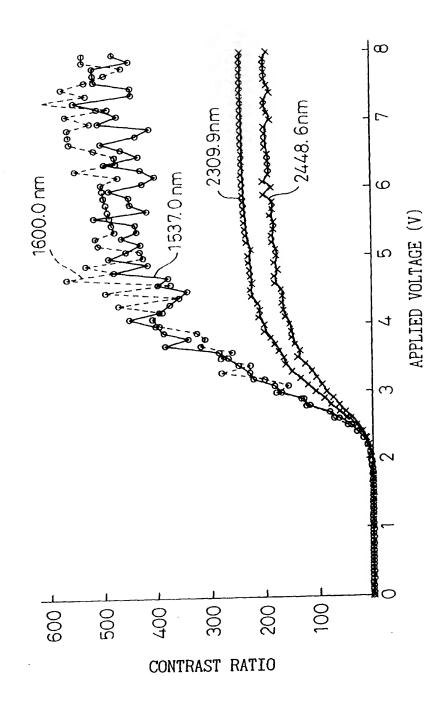
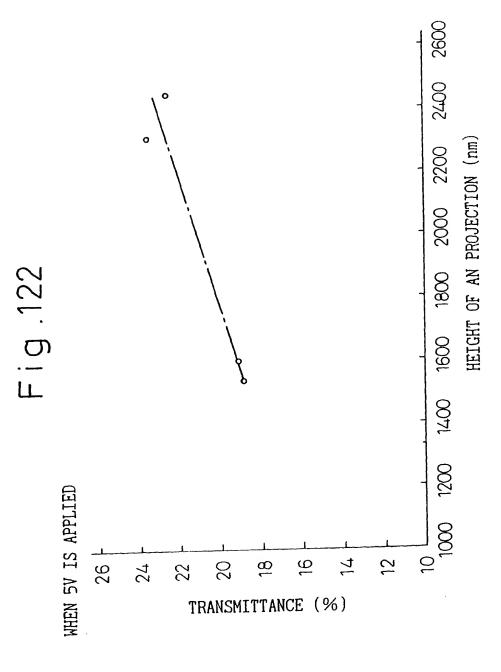
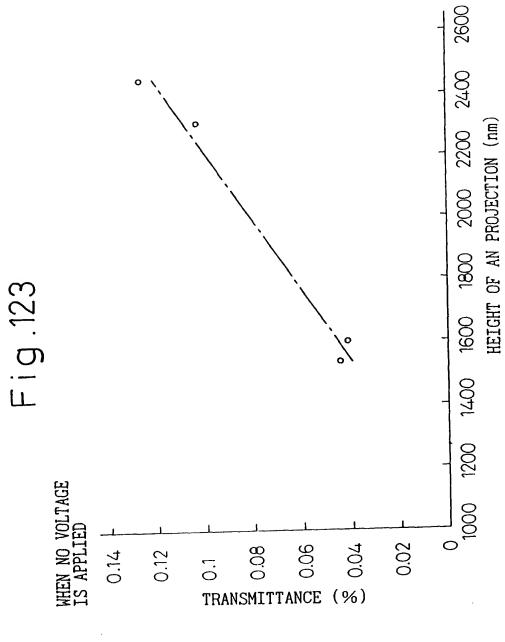


Fig.121









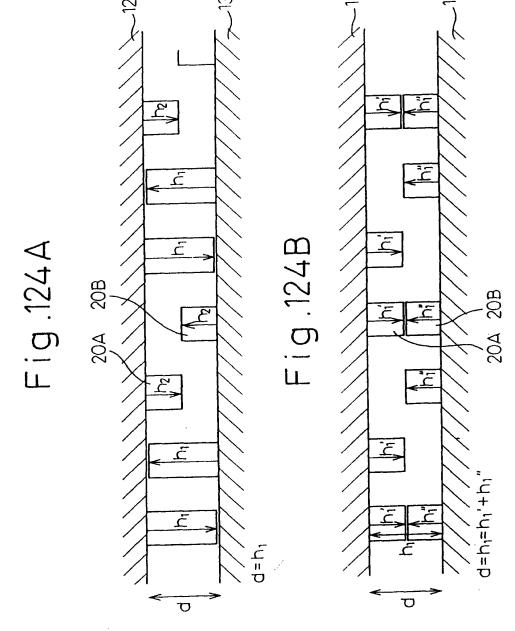


Fig.125A

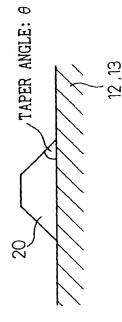
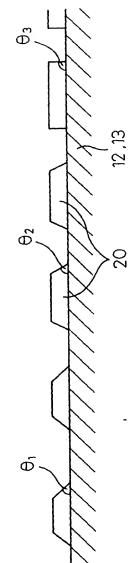


Fig.125B



 $\theta_1 < \theta_2 < \theta_3$



Fig.126

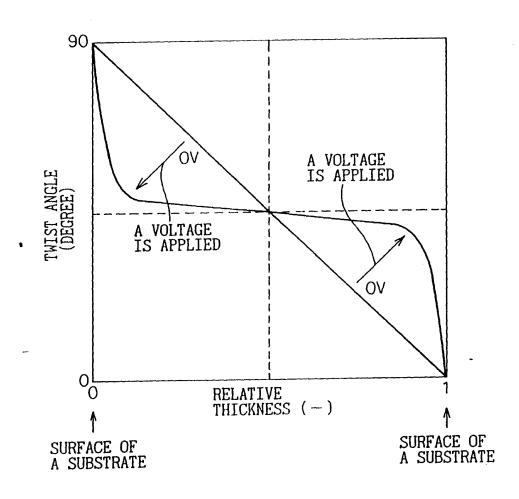




Fig. 127

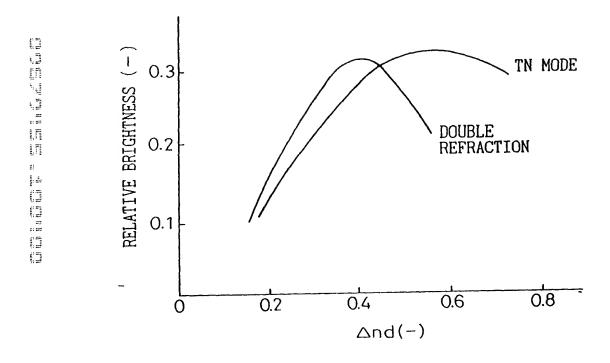
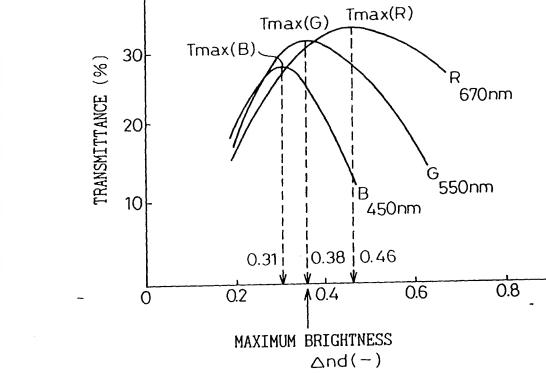


Fig.128



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Fig.129

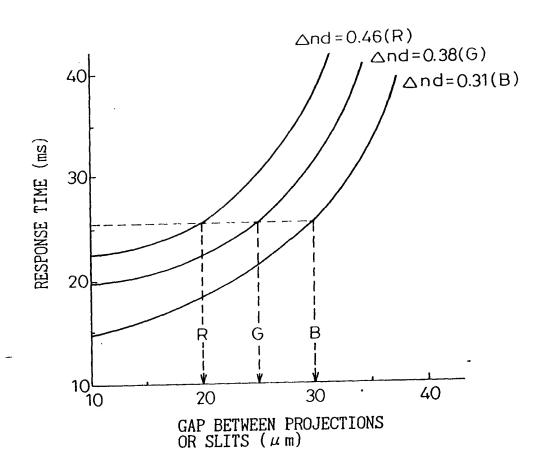
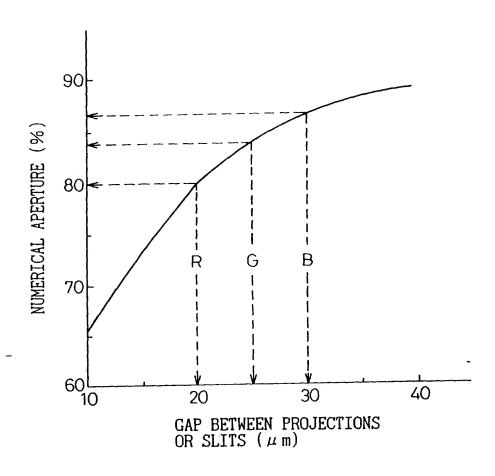
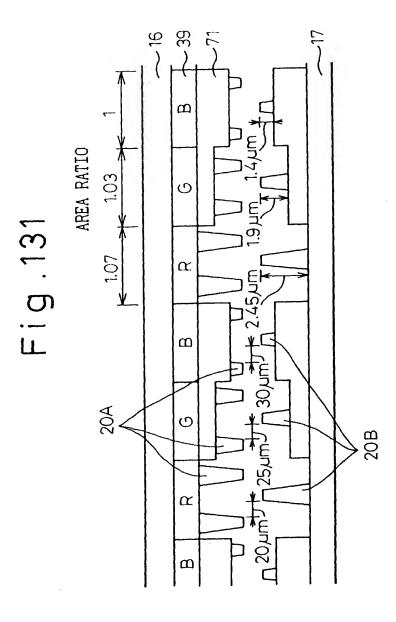


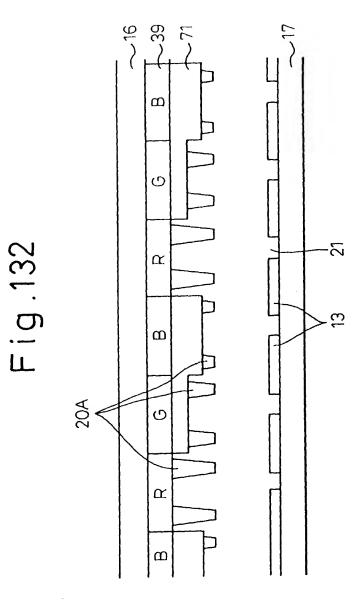
Fig.130



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Fig.133

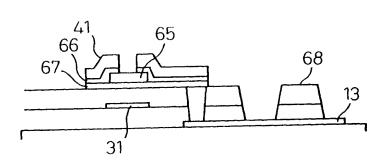
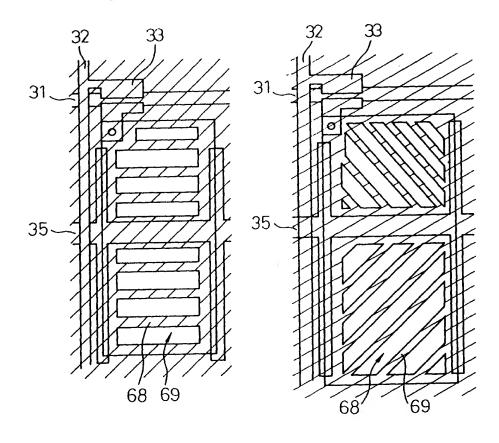


Fig.134A Fig.134B



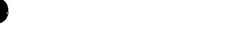
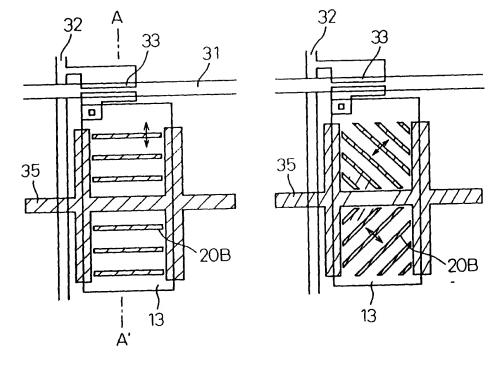


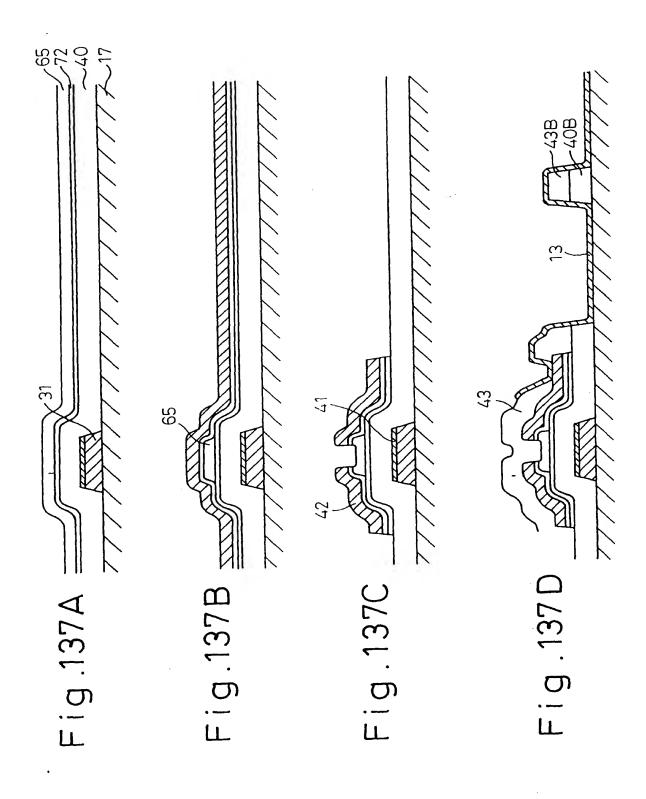
Fig.135 20B 7 7 8 a-Si / n+a-Si



Fig.136A Fig.136B

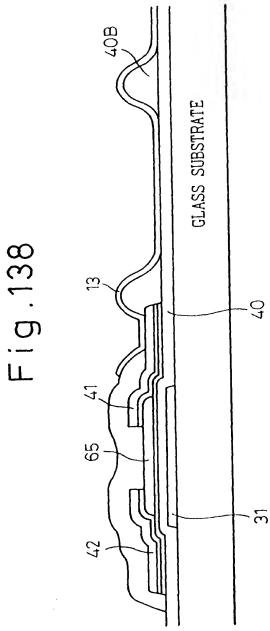




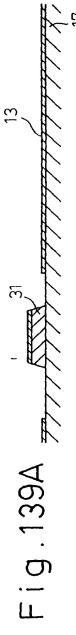


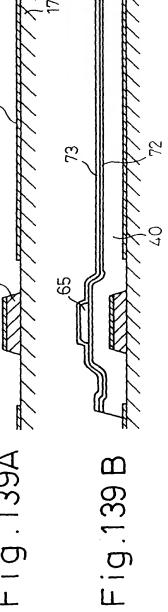


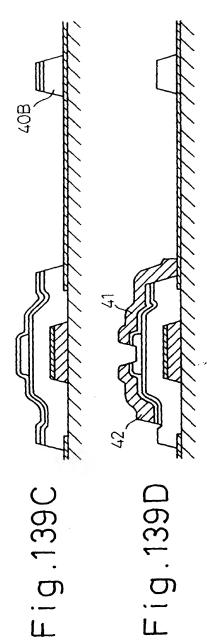
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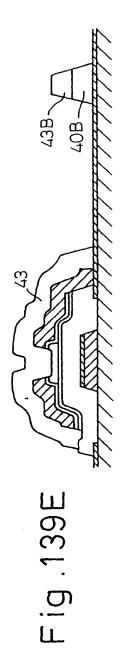




Fig.140A

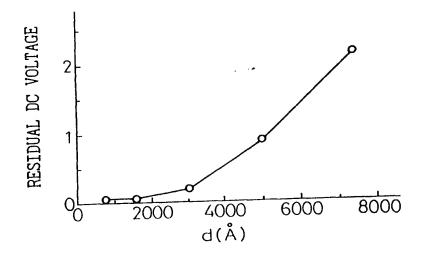


Fig.140B

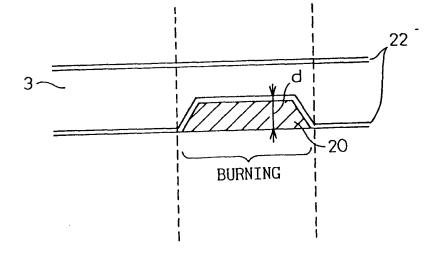




Fig.141A

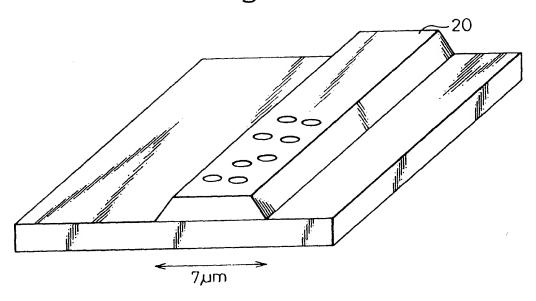
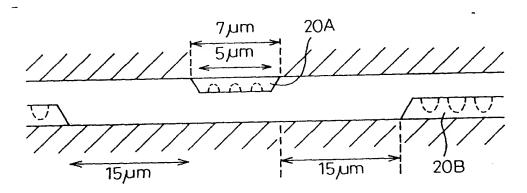


Fig.141B





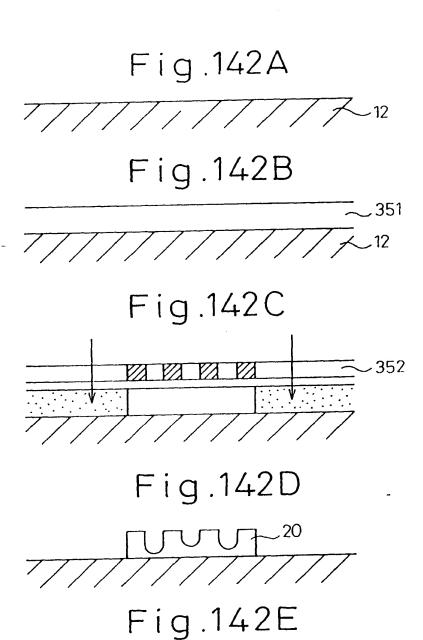
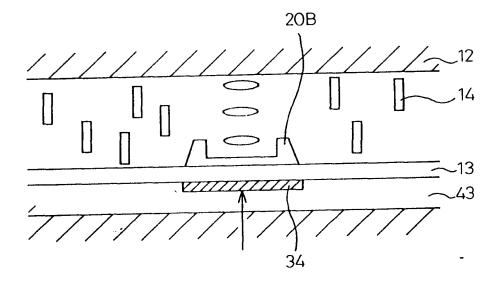
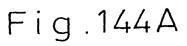




Fig.143





BEFORE BAKING

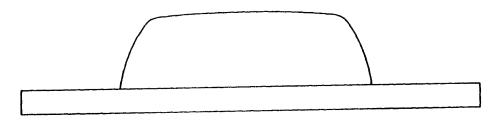
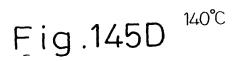


Fig.144B

AFTER BAKING







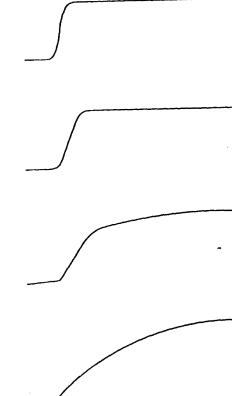


Fig.146A

2μm WIDTH

Fig.146B

Fig.146C



Fig.147A

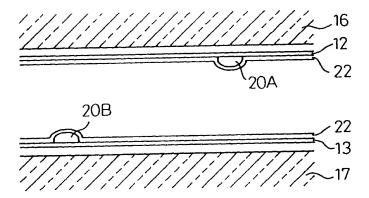


Fig.147B

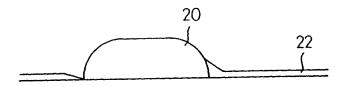




Fig.148A

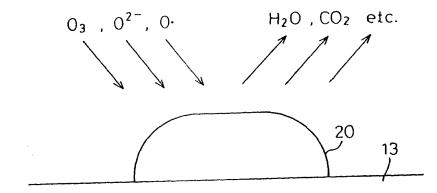


Fig.148B



Fig.148C

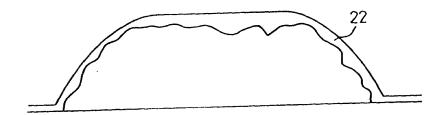




Fig.149A

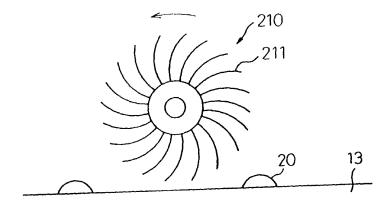


Fig.149B

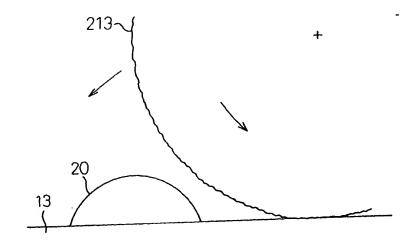






Fig.150

ULTRA-VIOLET LIGHT







Fig.151A

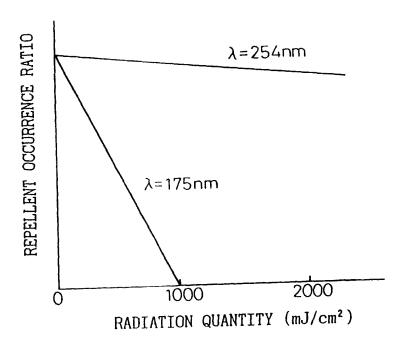


Fig.151B

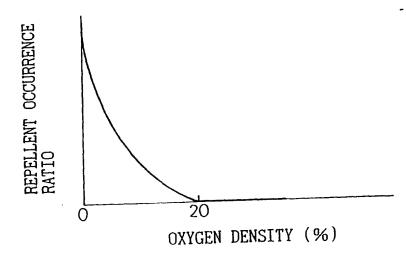




Fig.152A

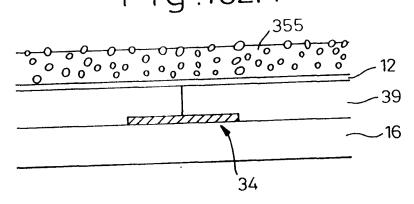


Fig.152B

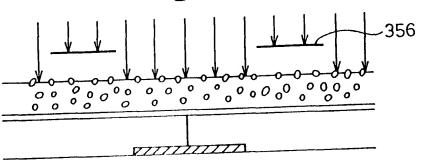


Fig.152C

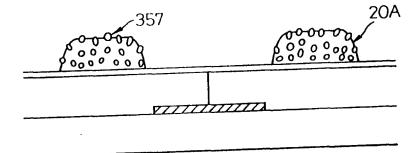




Fig.153A

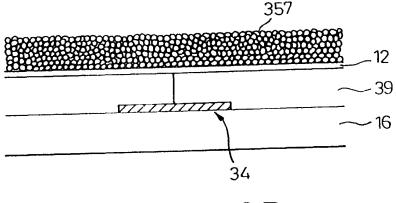


Fig.153C

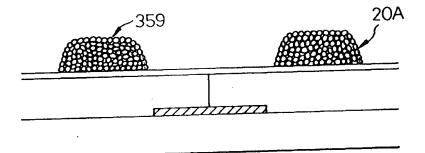




Fig.154A

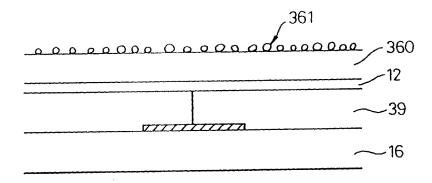


Fig.154B

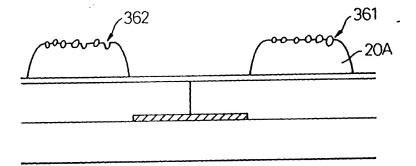




Fig.155A

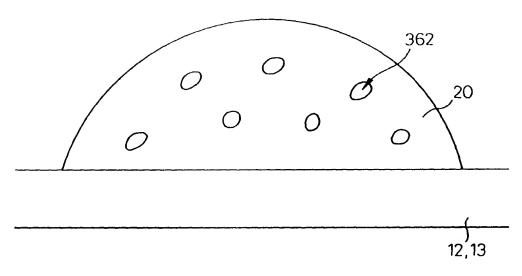
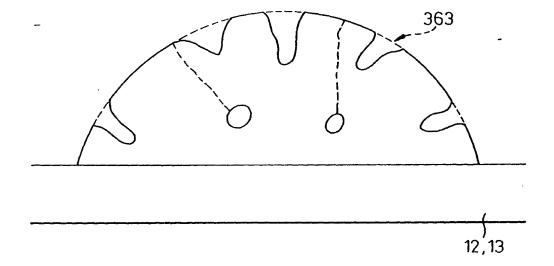
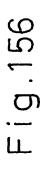


Fig.155B





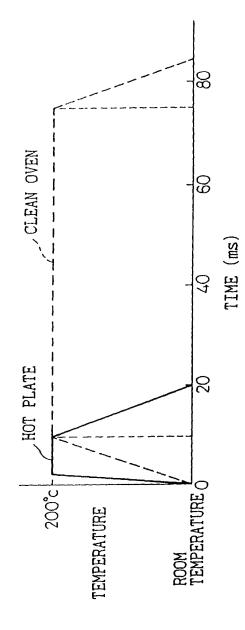




Fig.157A

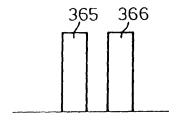
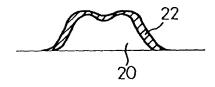


Fig.157B



Fig.157C





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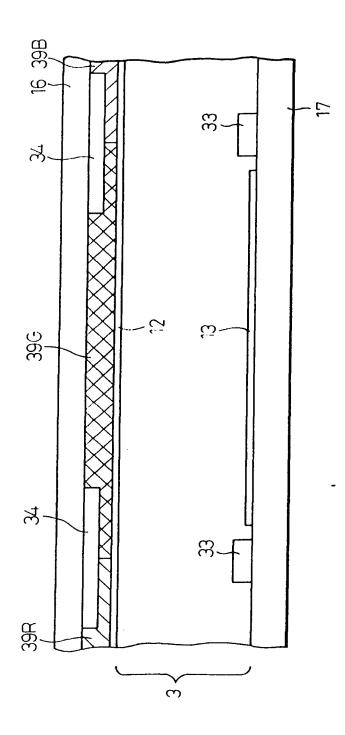


Fig.158

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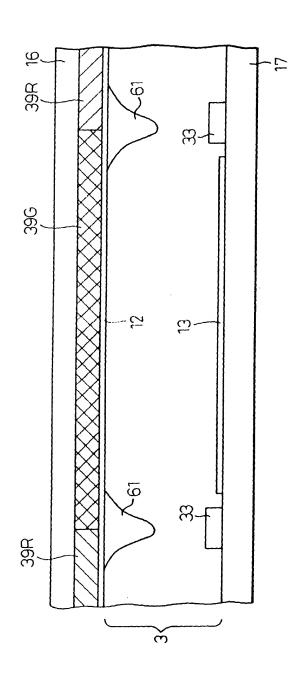
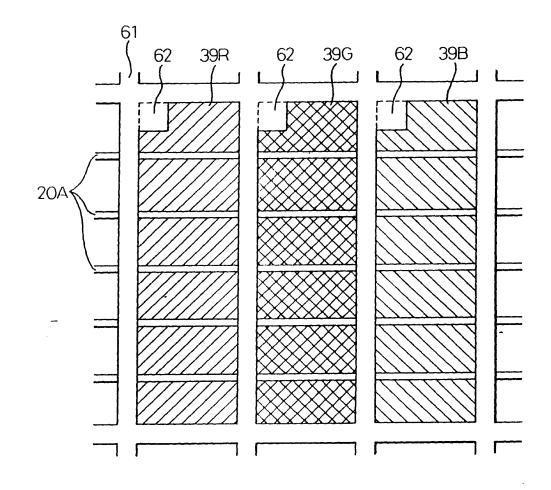


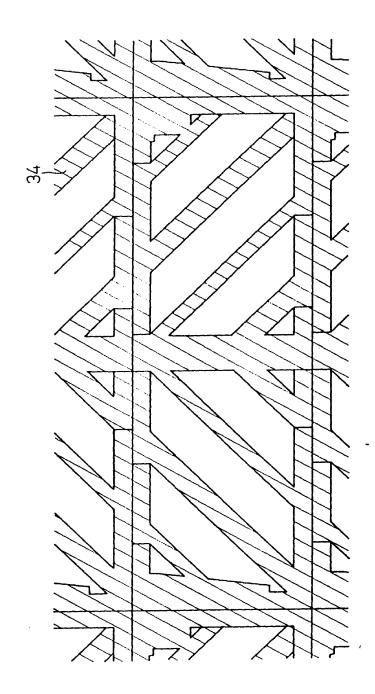
Fig.160



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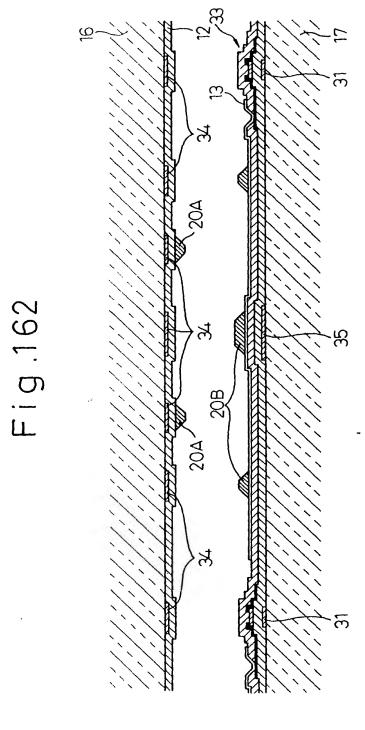
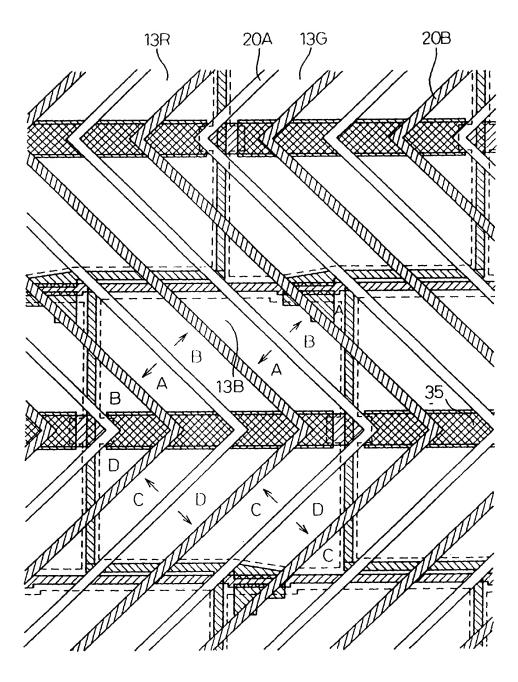




Fig.163



159 246

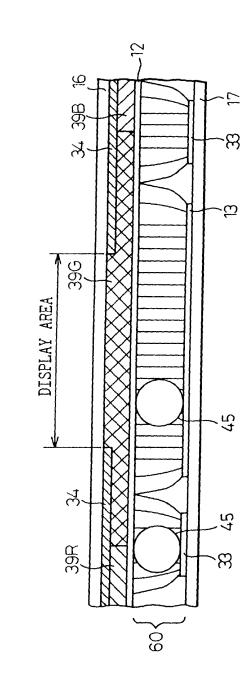
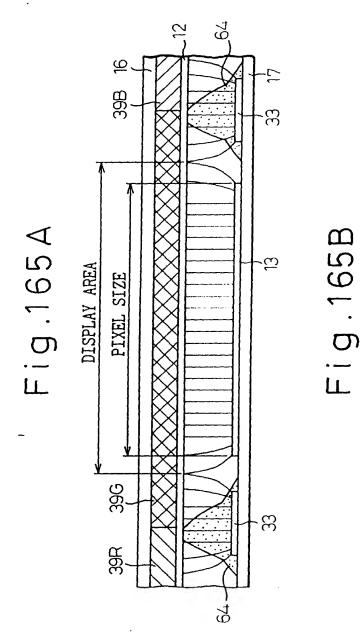


Fig.164

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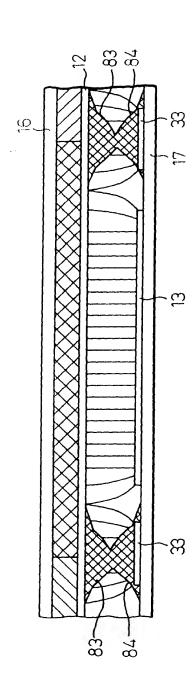


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85 8 ·Ж ഉ 9 3 Fig.166A Fig.166B 33, 45

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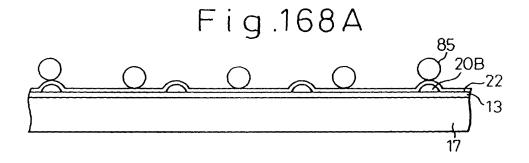


Fig.168B

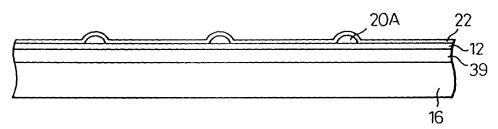
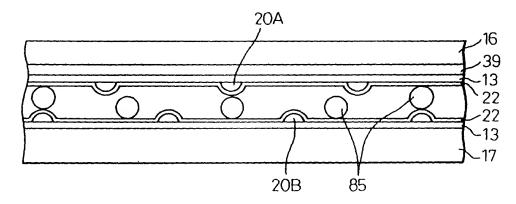
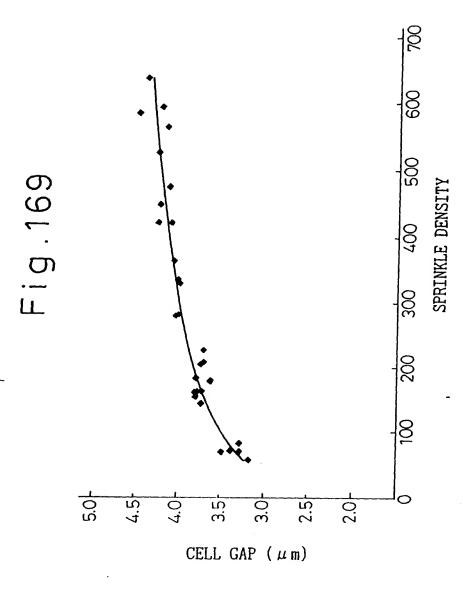


Fig.168C



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550 YES 2 500 YES 450 YES 웃 004 YES 2 350 YES 오 9 오 오 250 \mathfrak{L} 욧 200 S 9 <u>)</u> 잁 오 9 YES S YES 50 웃 SPRINKLE DENSITY OF SPACERS (NUMBERS/mm²) BLEMISH OCCURRENCE DUE TO PUSHING BLEMISH OCCURRENCE DUE TO PULLING



Fig.171A

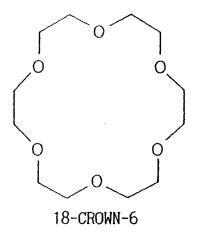
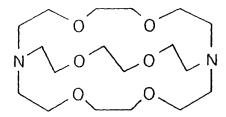


Fig.171B

DIBENZOYL-18-CROWN-6



Fig.172A



CRYPTAND [2.2.2]

Fig.172B

CRYPTAND [2.1.1]



Fig.173A

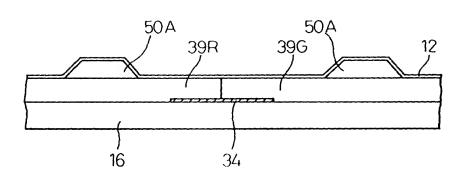


Fig.173B

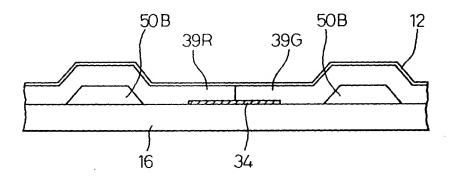




Fig.174

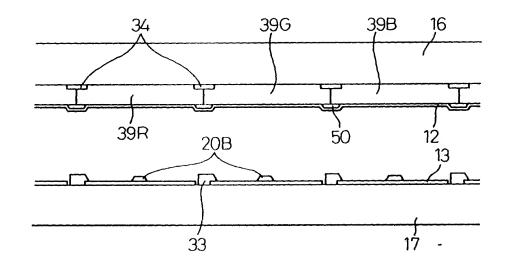


Fig.175A

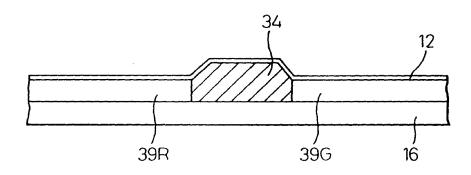


Fig.175B

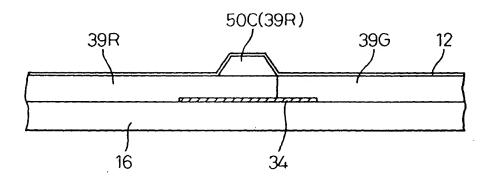




Fig.176A

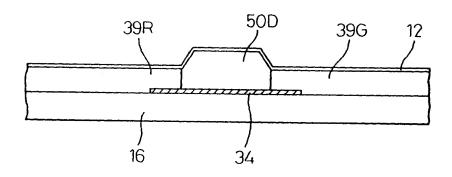


Fig.176B

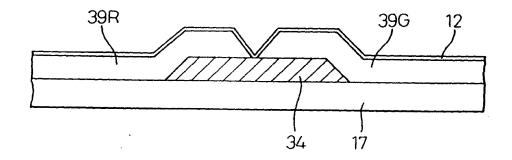




Fig.177A

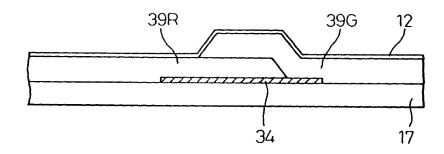
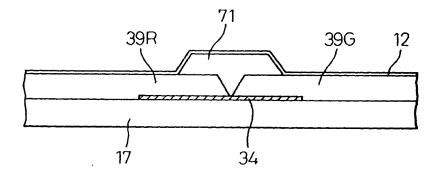


Fig.177B





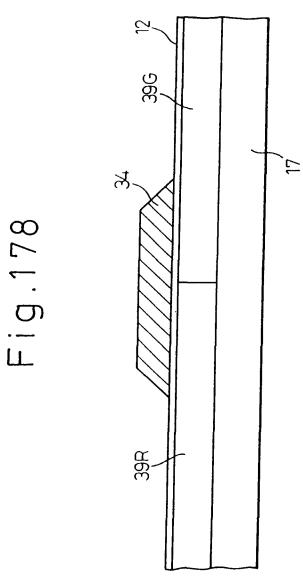




Fig.179A

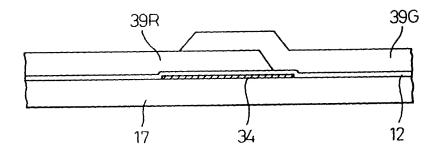
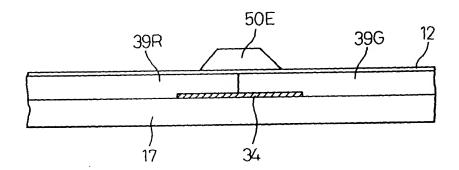


Fig.179B



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Fig.180A

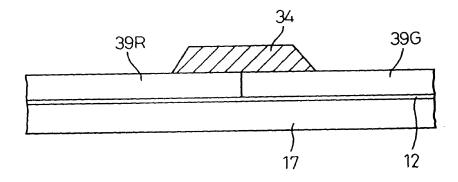
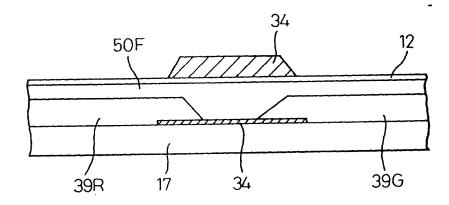
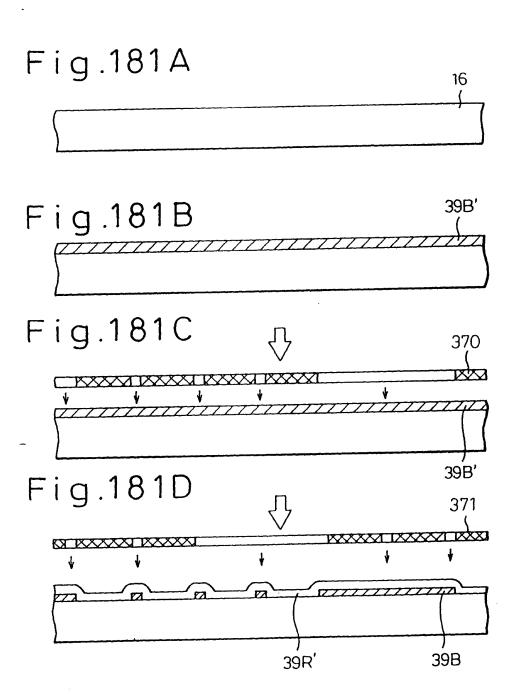


Fig.180B







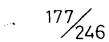


Fig.181E

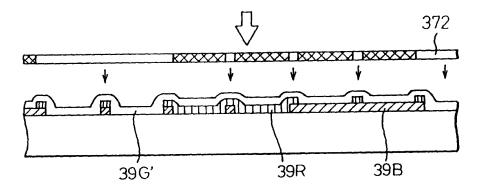


Fig.181F

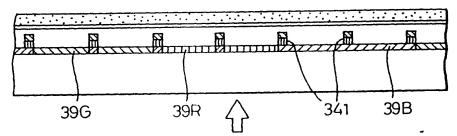


Fig.181G

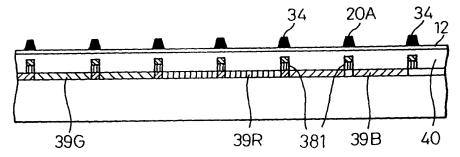
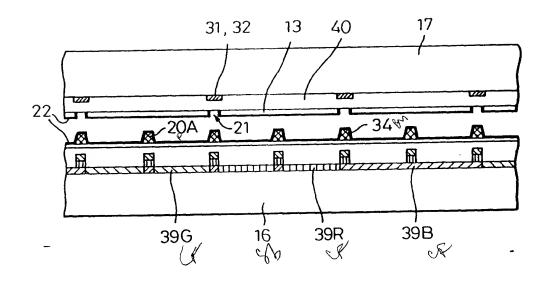


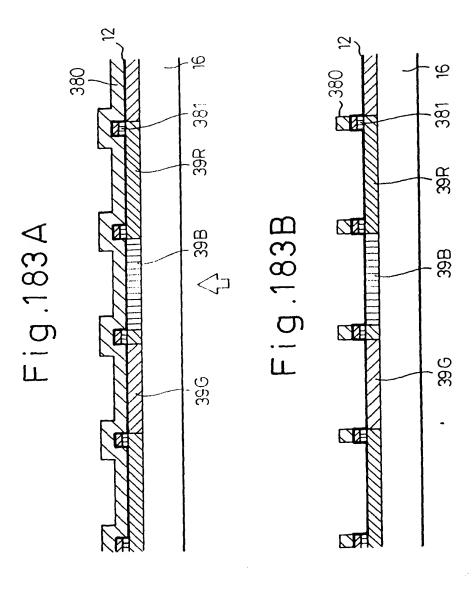


Fig.182



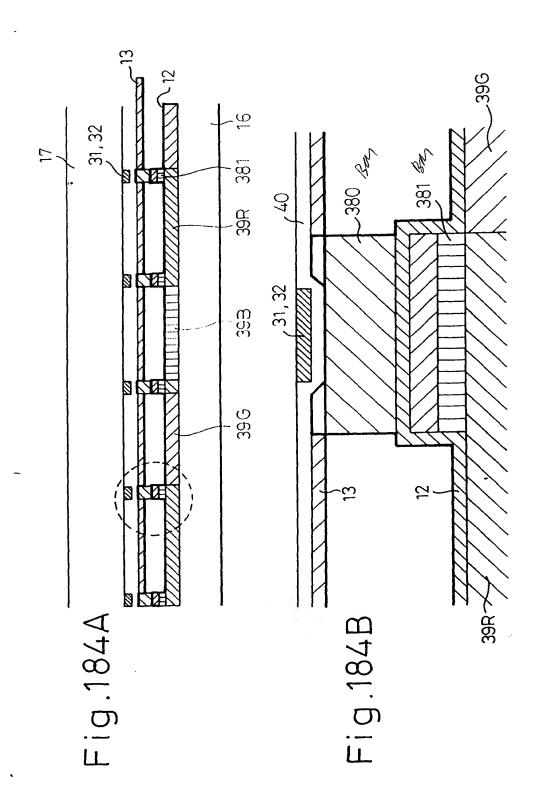


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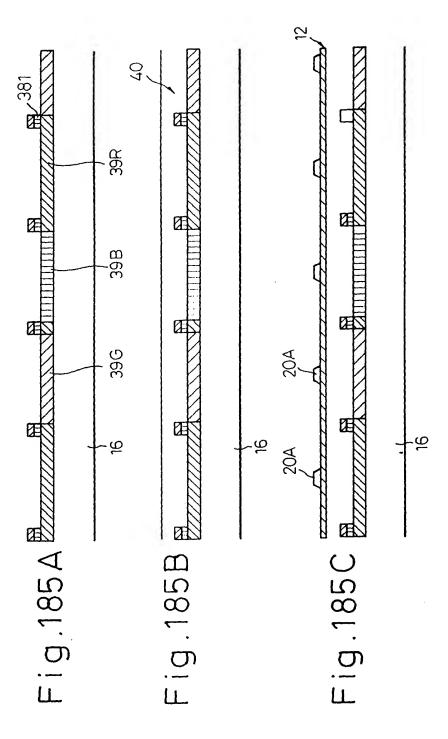


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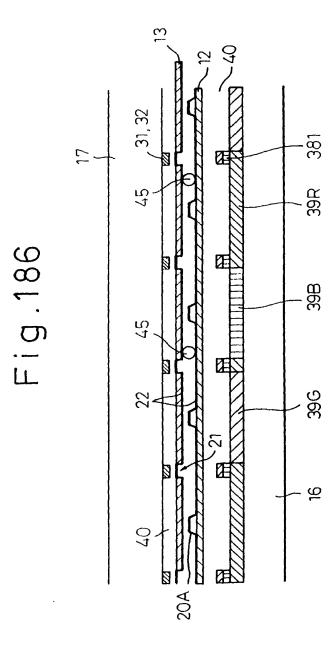


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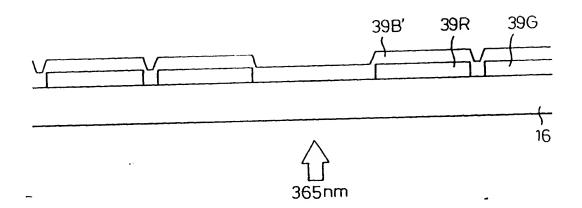




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Fig.187





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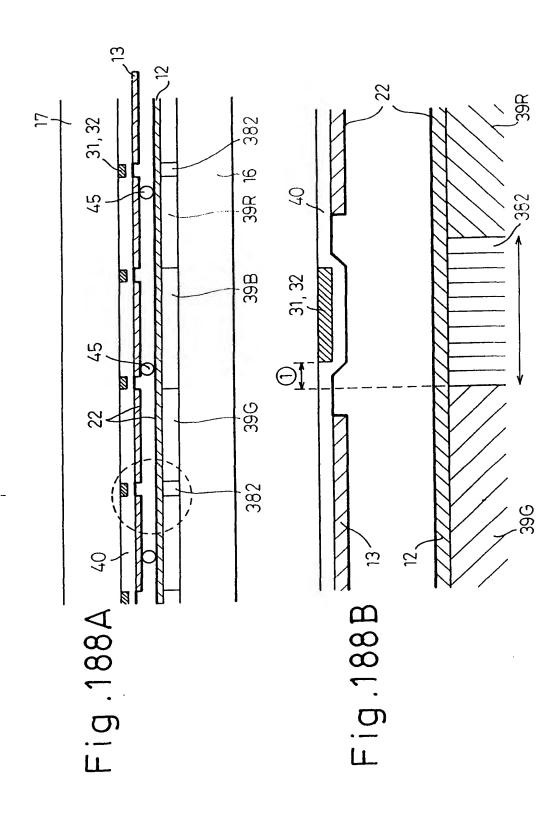




Fig.189

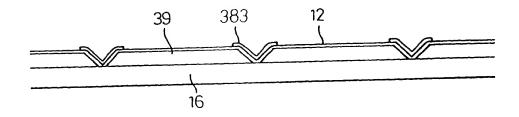


Fig.190A

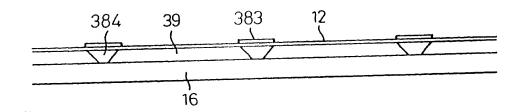


Fig.190B

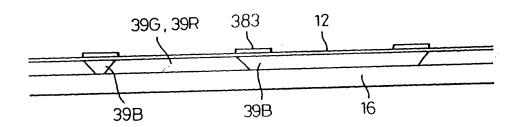




Fig.191

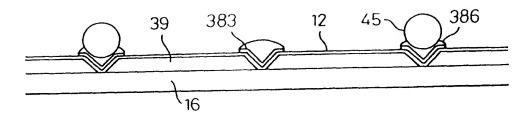


Fig.192

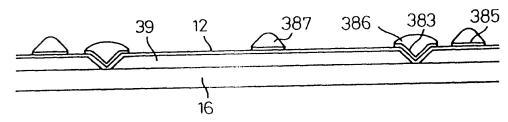


Fig.193

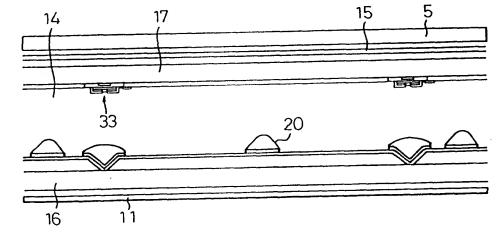




Fig.194

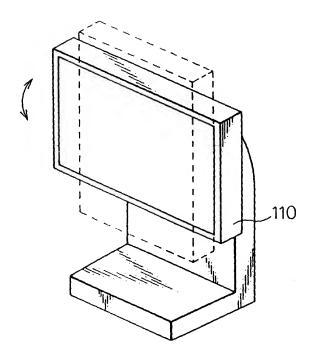


Fig.195

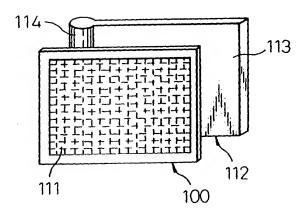




Fig.196A

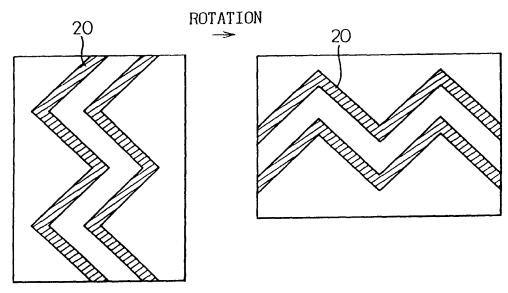


Fig.196B

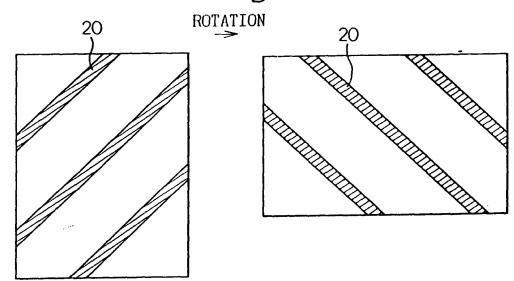
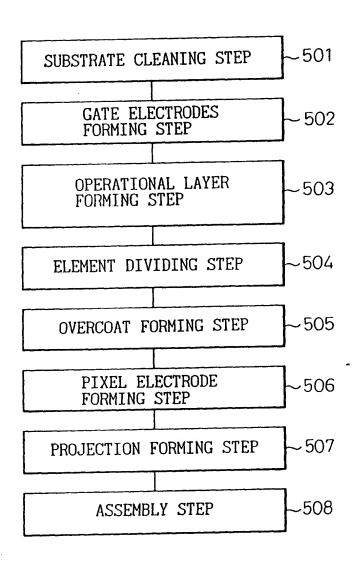






Fig.197



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Fig.198

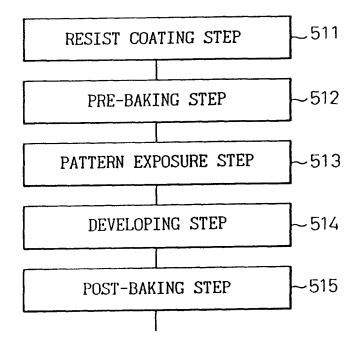
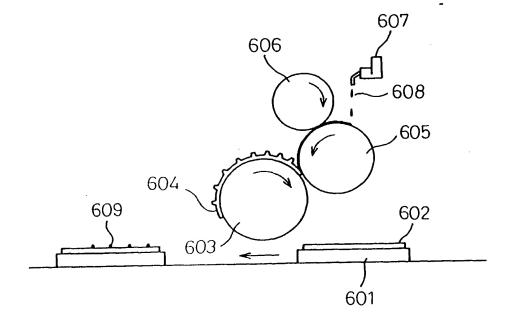


Fig.199





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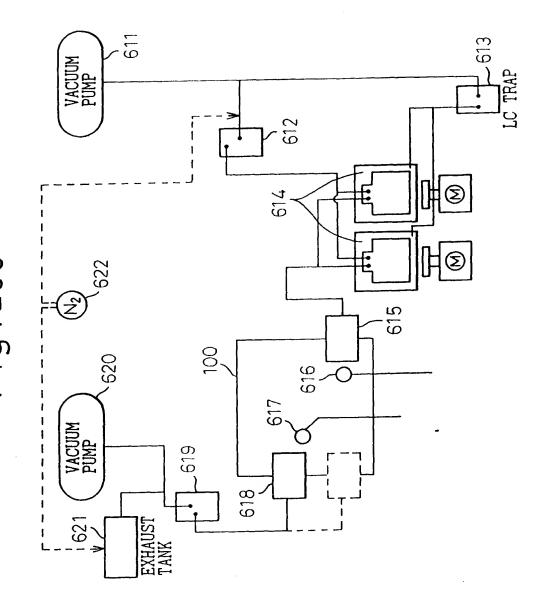


Fig.200



Fig. 201A

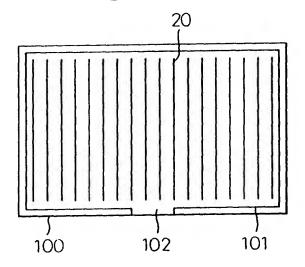
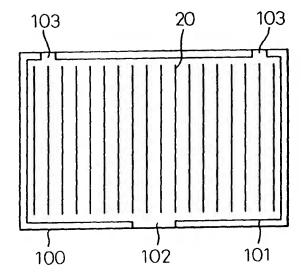


Fig.201B





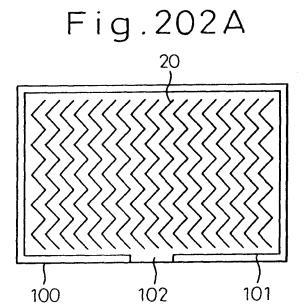


Fig.202B

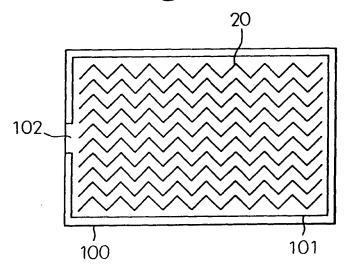




Fig. 203A

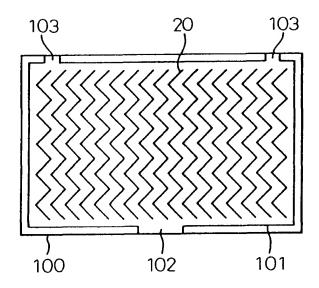


Fig.203B

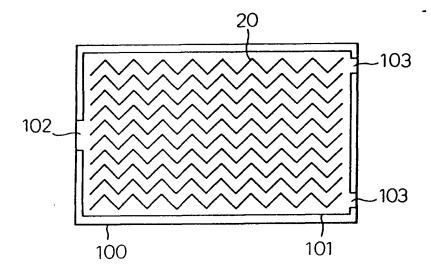




Fig. 204

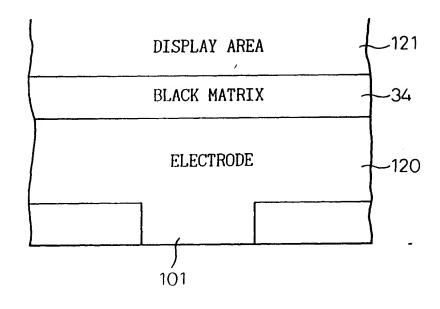
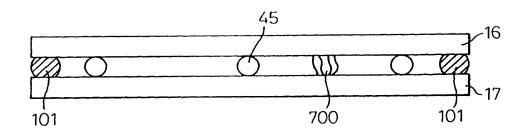






Fig.205A



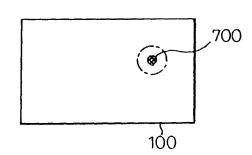


Fig.205B Fig.205C

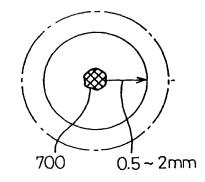


Fig.206

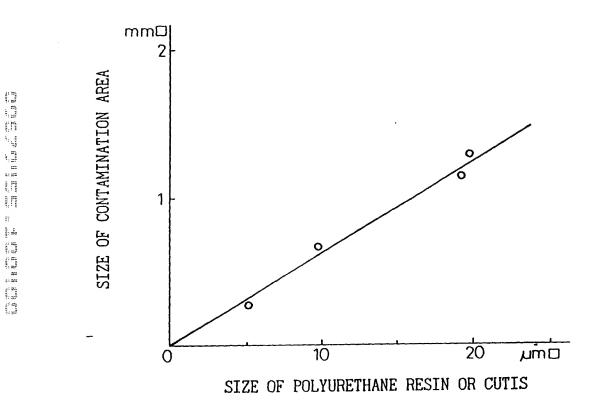
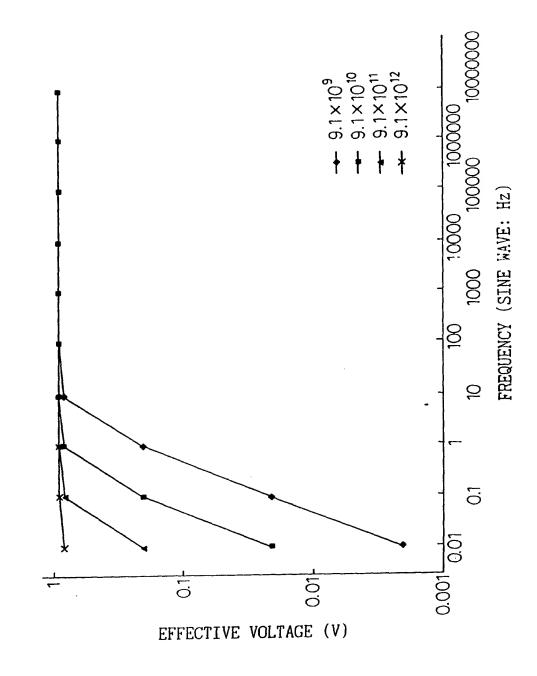
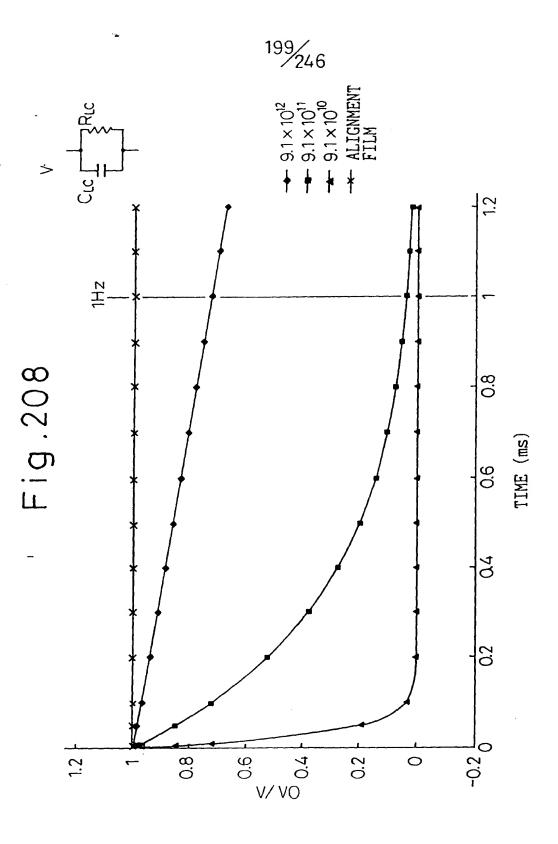






Fig. 207





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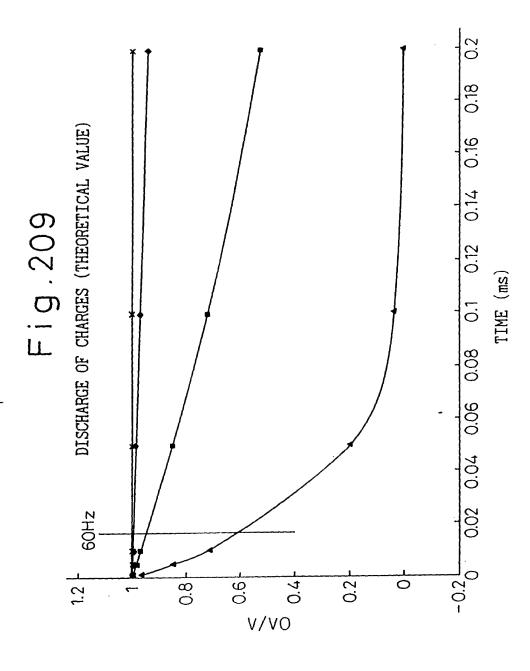






Fig.210

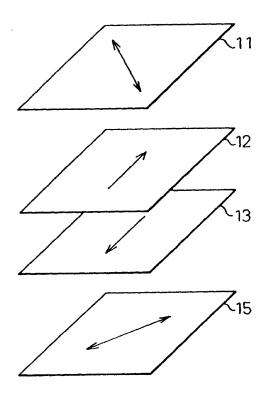




Fig.211

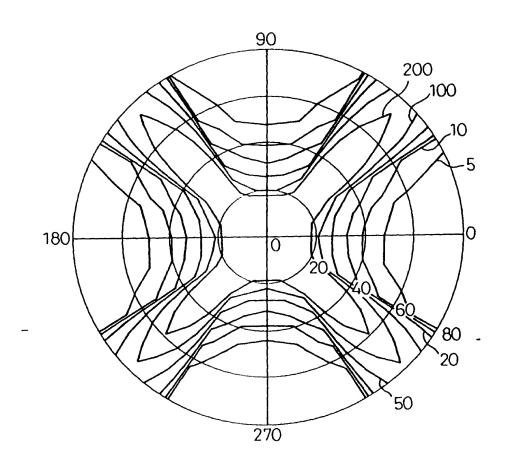
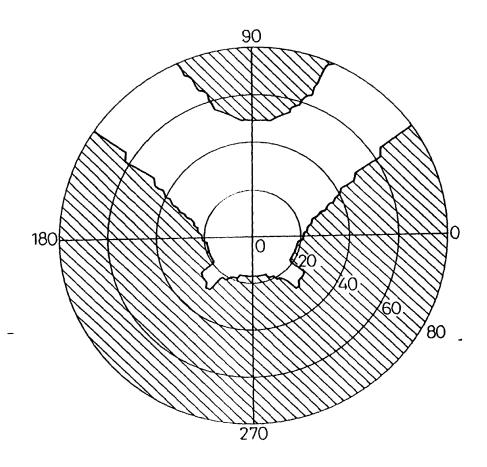




Fig.212







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Fig.213

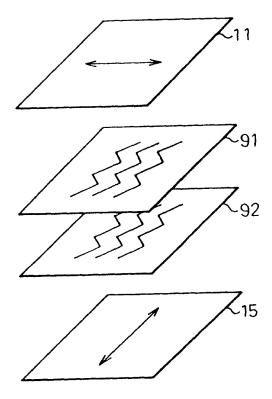




Fig. 214

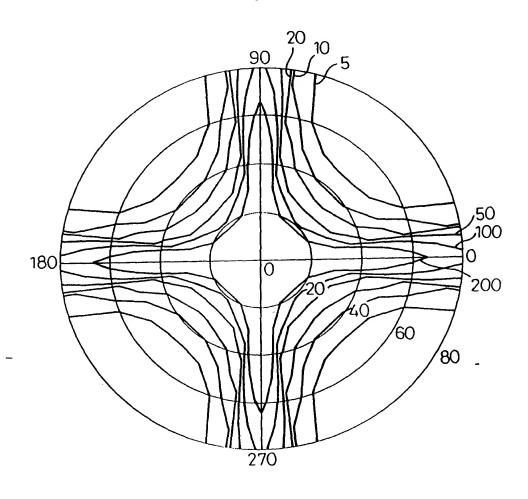




Fig.215

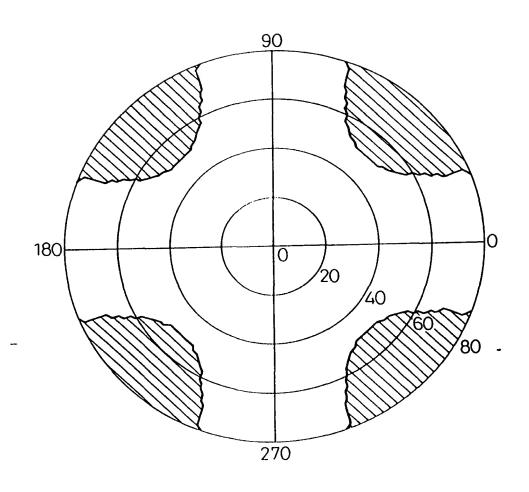
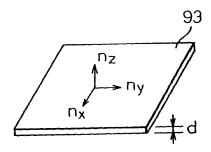




Fig.216



GENERAL CONDITION

POSITIVE UNIAXIAL FILM

NEGATIVE UNIAXIAL FILM

BIAXIAL FILM (A PHASE LAG AXIS IS X DIRECTION.)

RETARDATION IN INPLANE DIRECTIONS

RETARDATION OF THICKNESS DIRECTION n_x, n_y≥n_z

 $n_x > n_y = n_z$

 $n_x = n_y > n_z$

 $n_x > n_y > n_z$

 $R = (n_x - n_y)d -$

 $R = \left(\frac{n_x + n_y}{2} - n_z\right) d$



Fig. 217

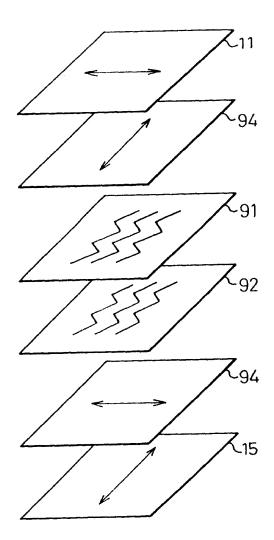




Fig.218

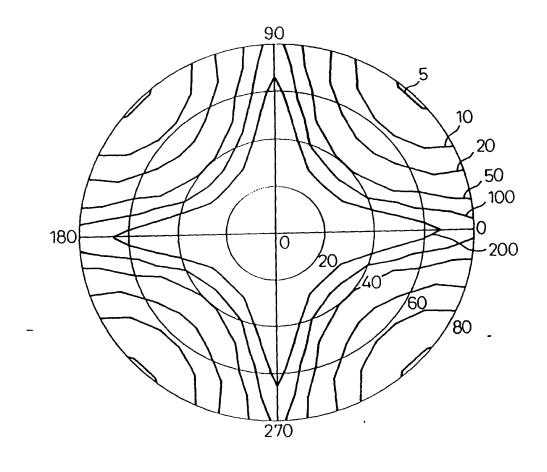
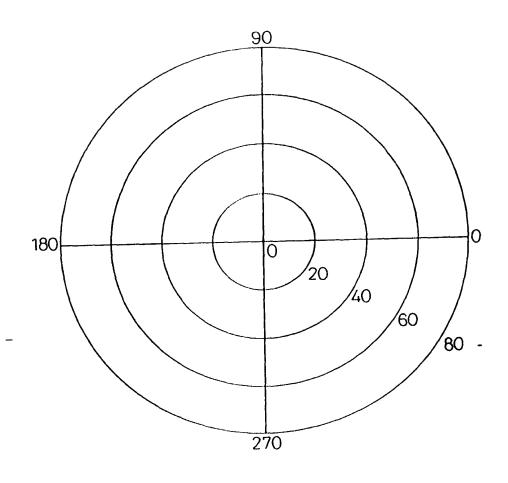




Fig.219





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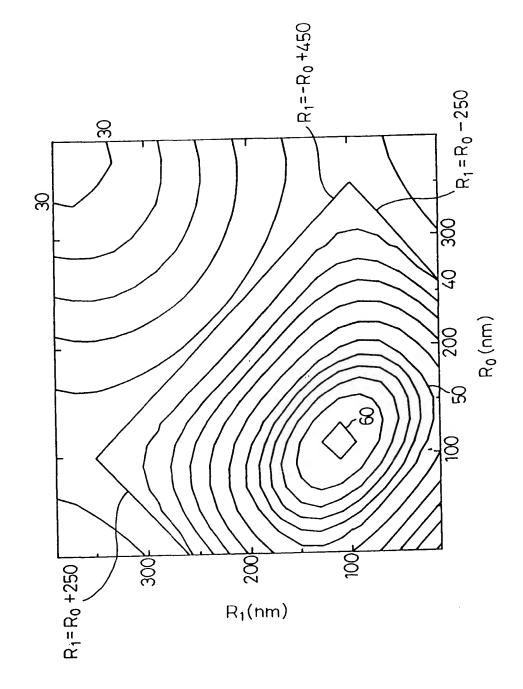


Fig.220

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Fig. 221

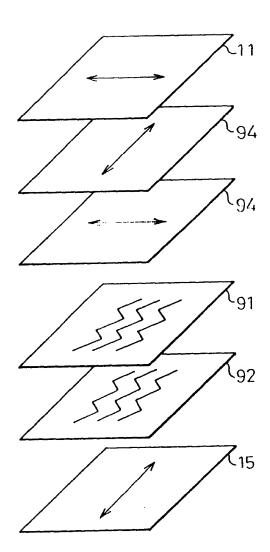




Fig. 222

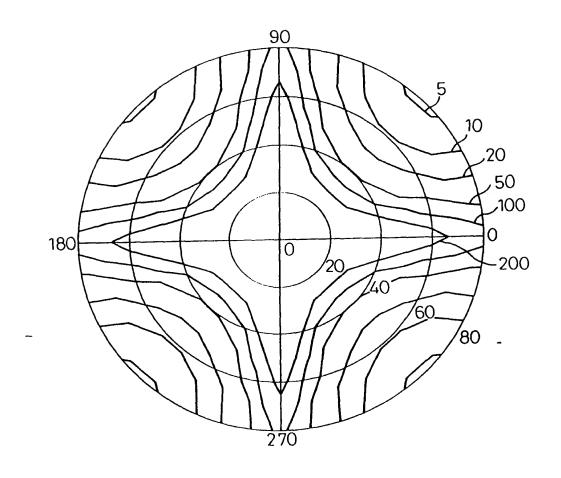




Fig. 223

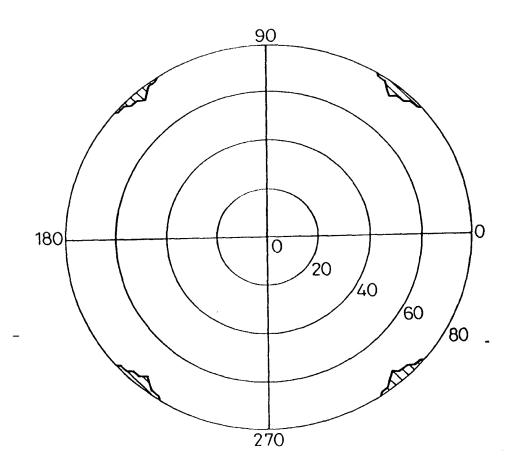




Fig.224

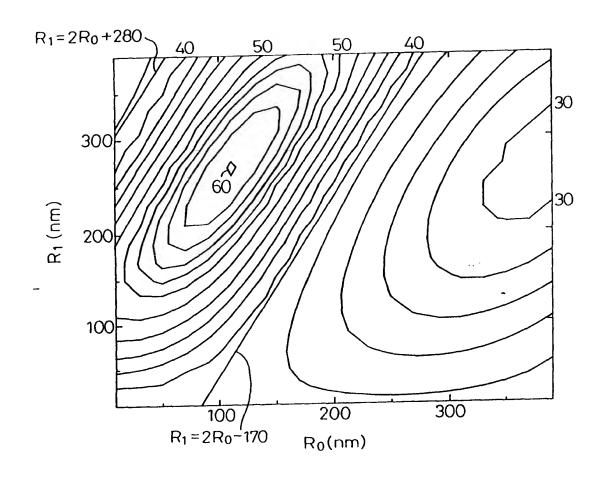




Fig. 225

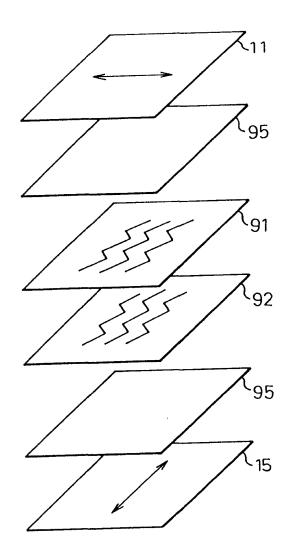




Fig.226

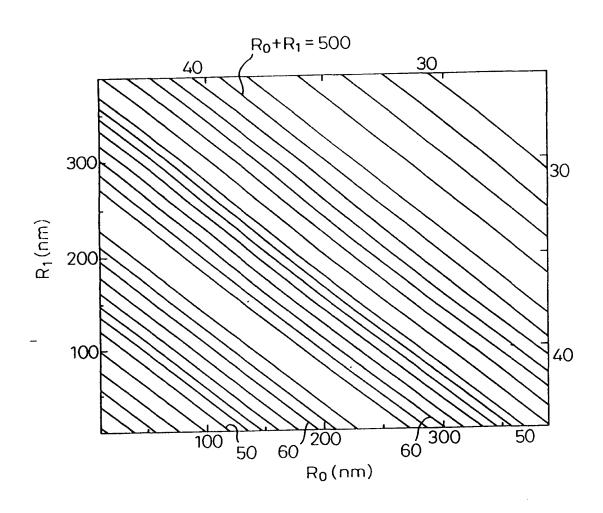




Fig.227

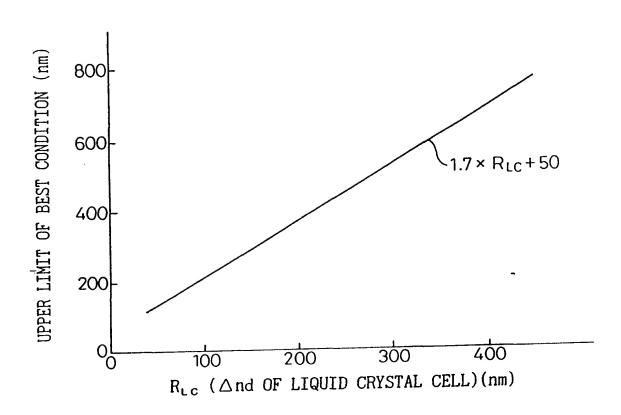




Fig.228

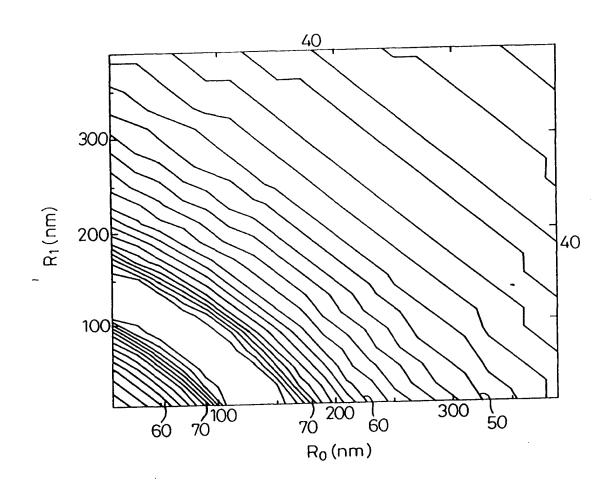




Fig.229

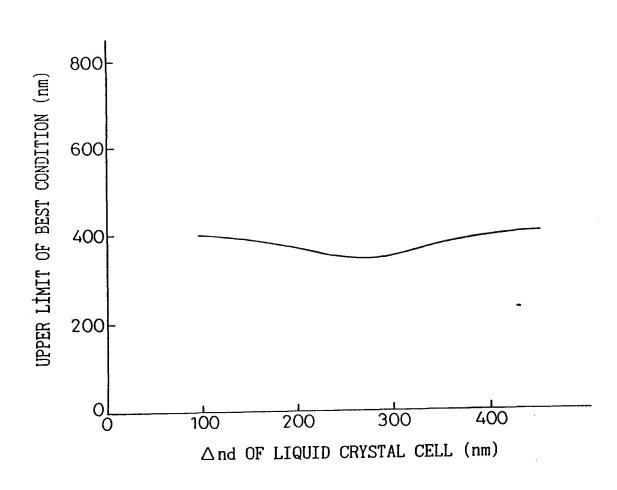


Fig.230

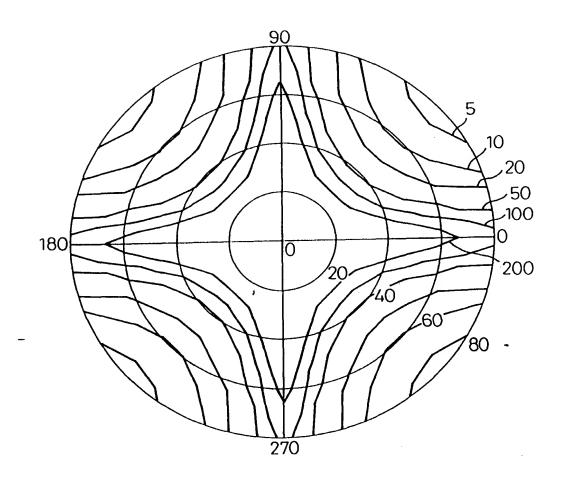


Fig. 231

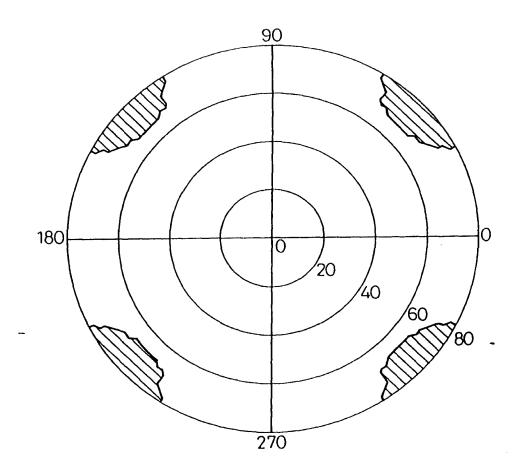




Fig.232

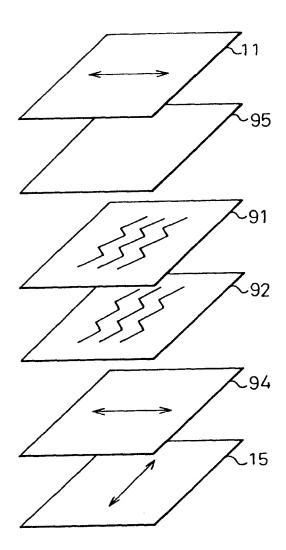




Fig.233

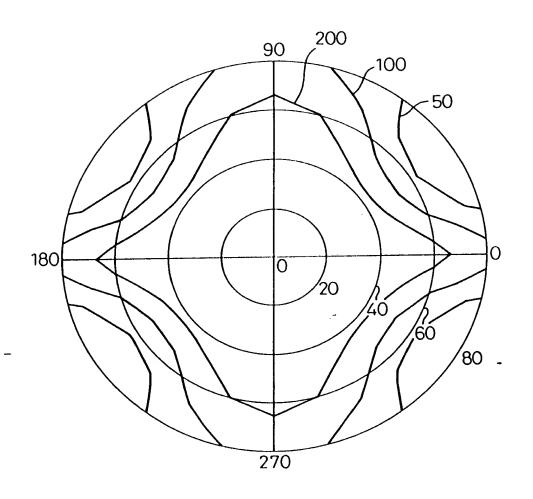




Fig. 234

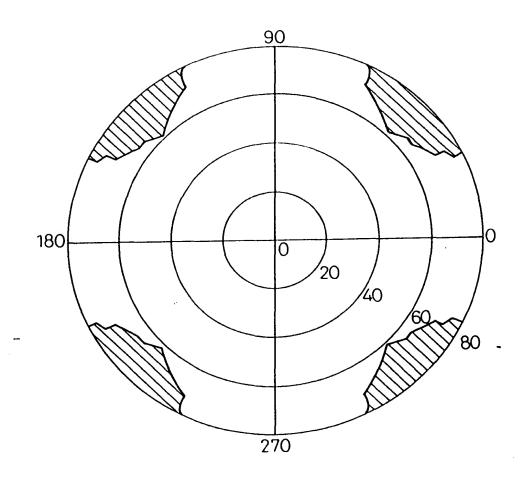




Fig.235

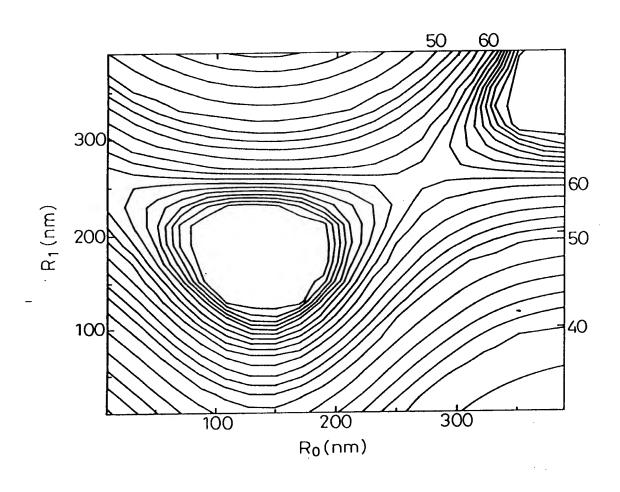




Fig.236

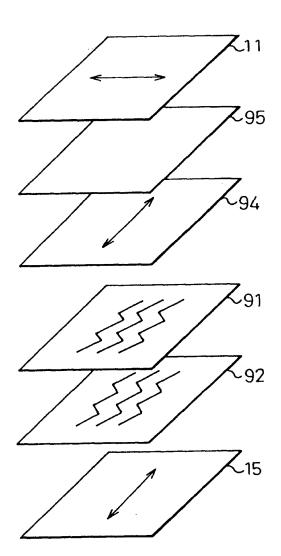




Fig.237

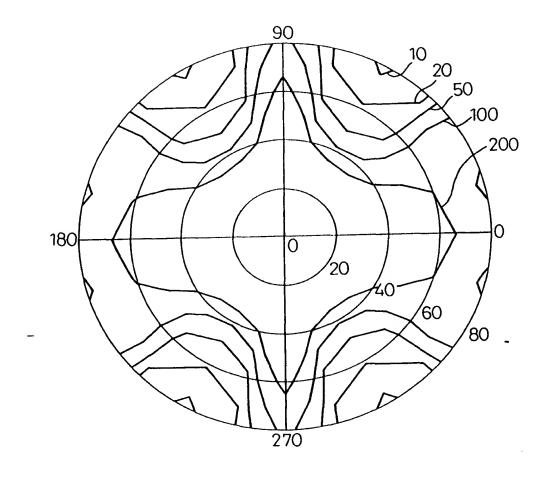




Fig.238

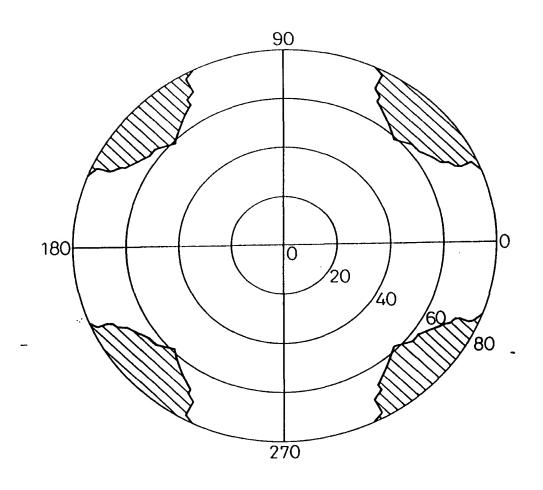




Fig.239

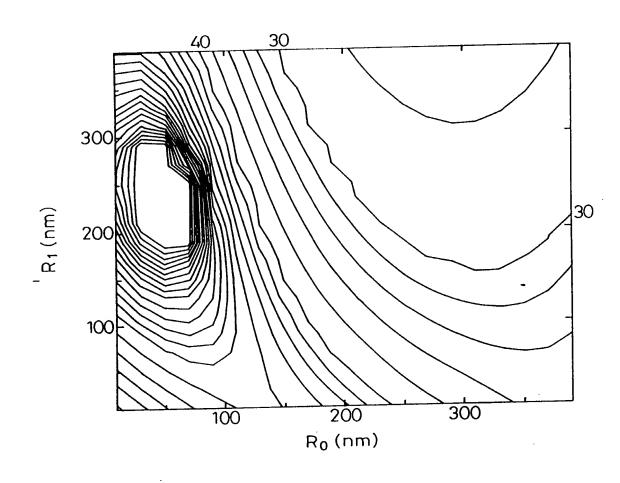




Fig. 240

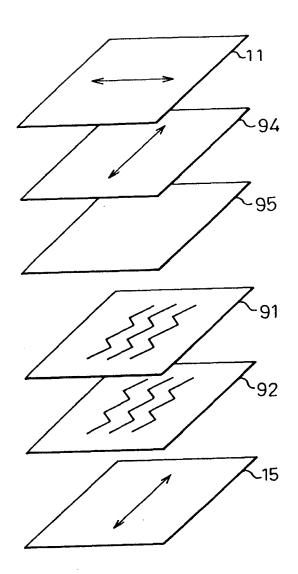




Fig.241

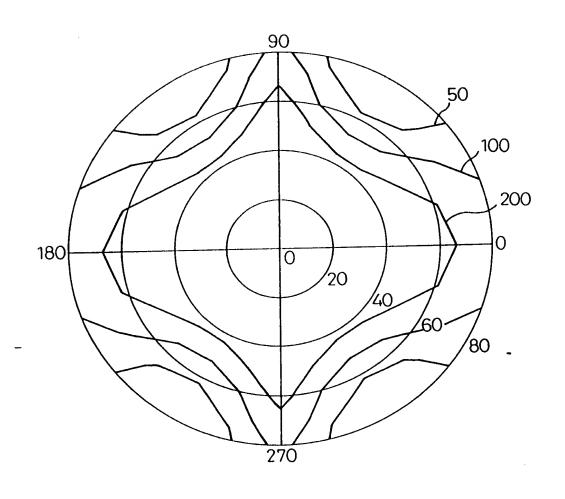




Fig.242

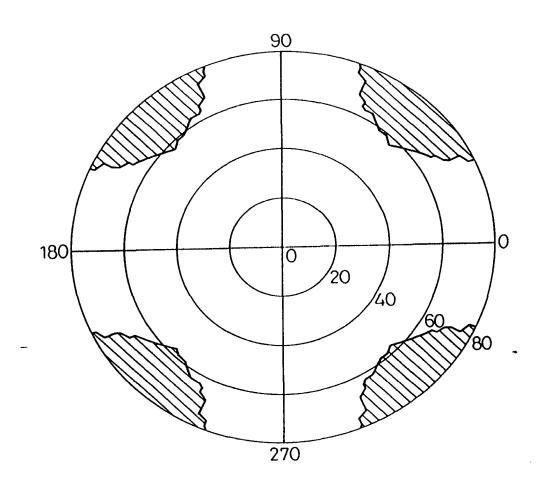




Fig.243

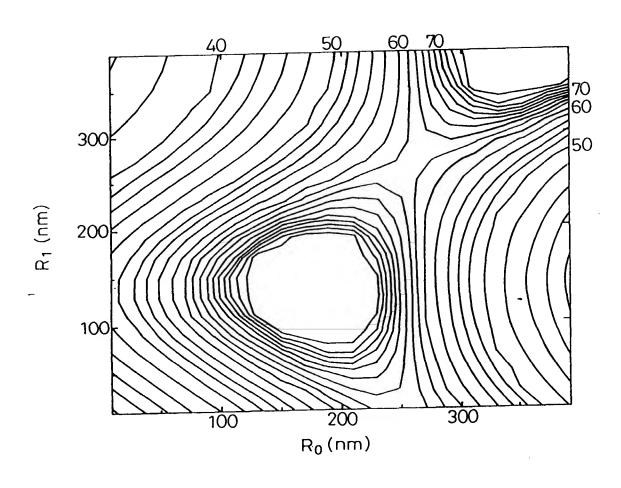
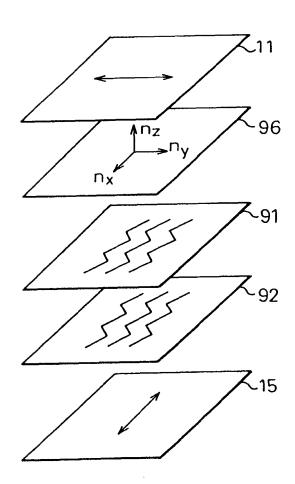


Fig. 244



The Court of the C



Fig.245

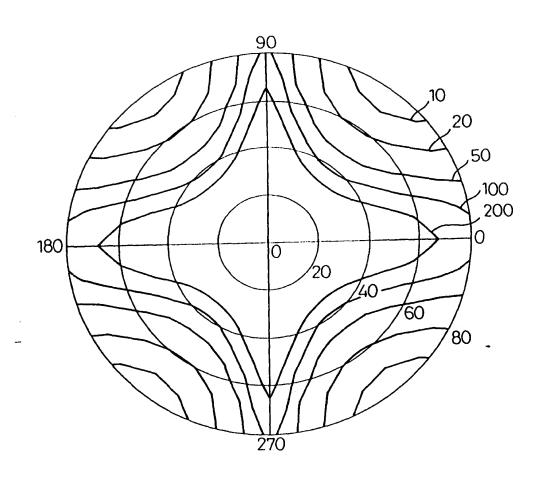
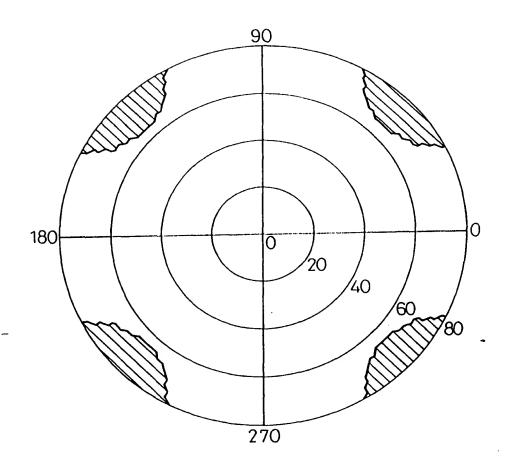






Fig. 246







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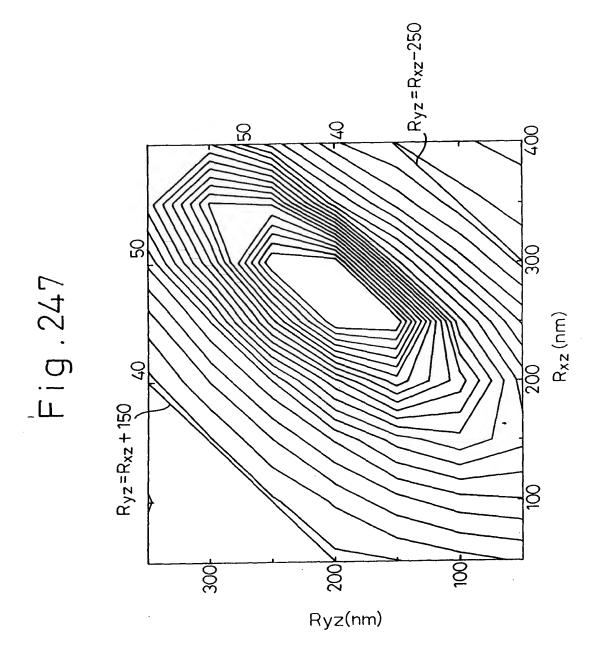
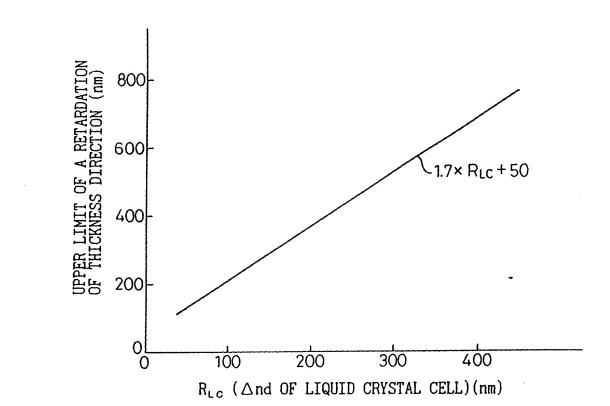


Fig.248



The bands of the first flags for the form of the first flags of the fl



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OLOR DIFFERENCE $\begin{pmatrix} 5v : LEFT \\ -RIGHT \end{pmatrix}$ $\triangle U(x) \mid \triangle V(Y)$		0.03	0.05	0.05	0.12
Ö		O.03	0.03	90.0	0.14
VIEW ANGLE : CR > 10 LEFT-RIGHT DIRECTION	0 0	O 8 H	+ 80°	+ 80°	+ 80.
TRANS- MITTANCE 96 (5v)		کو.د م	5.60	4.50	5.80
PHASE DIFFERENCE FILM Rd VALUE (nm)		320	320	240	320
GAP BETWEEN PROJECTIONS (μm) R G B		20, 25, 30	20, 25, 30	R, G, B=30	R, G, B=30
THICKNESS OF A PANEL (\(\mu \) R G B	() () ()	5.7, 4.6, 3.6	5.7, 4.6, 3.6	PRIOR ART R,G,B=3.6	PRIOR ART R,G,B=4.6
SAMPLE	EMBODIMENT	¥	EMBODIMENT 5.7, 4.6,	PRIOR ART	PRIOR ART

Fig. 249





Fig. 250

EXAMPLES	INITIAL VALUES	AFTER 200 HOURS	
EMBODIMENT C	25	42	
EMBODIMENT D	33	51	
EMBODIMENT E	26	45	
EMBODIMENT F	30	48	
REFERENCE	32	70	



Fig.251A

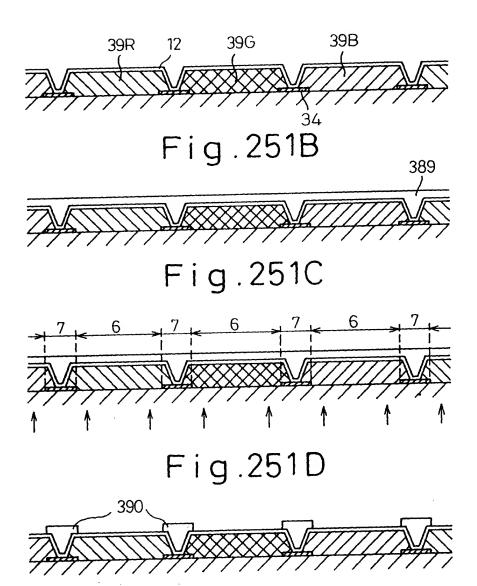




Fig.252A

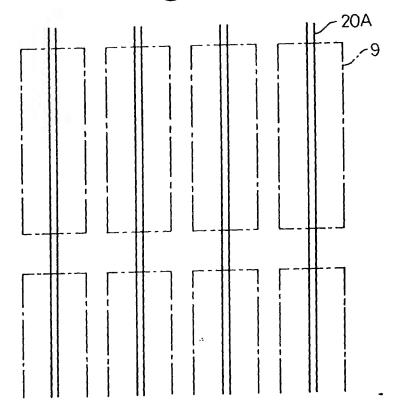
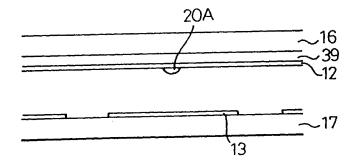


Fig.252B

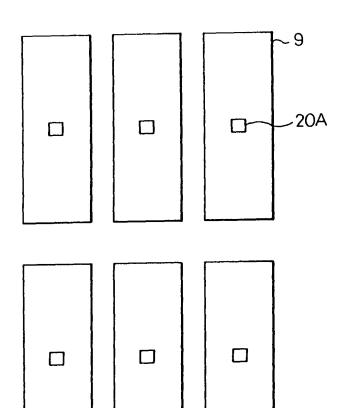






²⁴⁴/₂₄₆

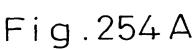
Fig. 253







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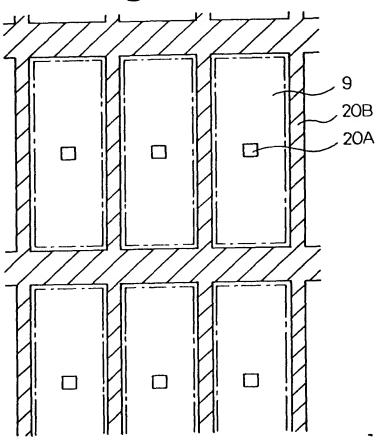
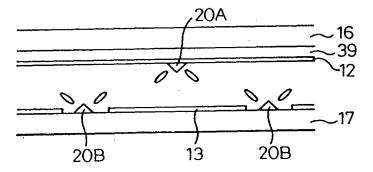


Fig.254B







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Fig.255

